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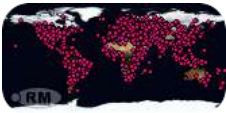
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ABSTRACT AND REFERENCES

APPLIED MECHANICS

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OPTIMIZATION OF THE SOLAR CELL BASED ON CADMIUM TELLURIDE BY ADDING THE CdSeTe ABSORBING LAYER (HETEROSTRUCTURE SIMULATION) (p. 6–12)

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Cadmium telluride solar cells are among the most common devices for photovoltaic applications. However, the energy conversion efficiency of these elements remains insufficiently high. Using the SCAPS programming environment, research and optimization of a classical thin-film solar cell based on CdTe were carried out. The structure of this element consisted of ITO as a transparent conductive contact, a cadmium sulfide (CdS) layer, and a cadmium telluride (CdTe) absorber layer with a metal contact. To optimize this structure in terms of power conversion efficiency, the influence of the thickness and concentration of acceptor impurities in the CdTe absorbing layer, as well as the influence of the thickness and concentration of donor impurities in the CdS buffer layer, were considered. It was established that the optimal thicknesses for the CdS buffer layer and absorption CdTe layers are 50 nm and 3000 nm, respectively. An additional CdSeTe layer between the CdS and CdTe layers has been proposed as one of the optimization options to improve the device efficiency. The main photovoltaic parameters of such a solar cell were analyzed depending on the thickness of the CdSeTe layer and its selenium content. It has been demonstrated that adding CdSeTe solid solution to the 1500 nm thick CdTe absorber layer increases the efficiency of the solar cell by 6.84%. The main photovoltaic characteristics of CdS/CdTe and CdS/CdSeTe/CdTe solar cells were compared. The results showed that the simulated CdS/CdSeTe/CdTe structure provides better photoconversion efficiency in the AM1.5G light spectrum compared to the classical CdS/CdTe structure. Such elements can be used to form highly efficient solar panels.

Keywords: solar cell, SCAPS, thin films, heterostructures, cadmium telluride, cadmium chalcogenide.

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ASSESSING THE POTENTIAL ACCURACY OF A SMALL-SIZED GONIOMETER WITH EXTENDED DYNAMIC RANGE BASED ON NUCLEAR MAGNETIC RESONANCE (p. 13–25)

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This paper evaluates potential accuracy characteristics of a small-sized goniometer based on nuclear magnetic resonance with an extended dynamic range. This required constructing a model of goniometer errors, estimating its accuracy based on this model, and formulating practical recommendations for the design of such a device based on the accuracy assessment.

To evaluate the accuracy of a nuclear goniometer, a theoretical model was built that makes it possible to determine the optimal operating parameters of the cell gas mixture, the ranges of their permissible changes, the sensitivity of the goniometer, and the dependence of its characteristics on external and internal factors. In particular, the dependence of output signal of the device on the parameters of gas mixture and optical pumping has been determined. For a goniometer with a cell volume of 8 cm³, the optimum temperature is 130 °C, and the optimum intensity of the pumping radiation is 5 mW.

The dependence of output signal on the measured angle of rotation was also established, as well as the noise and error dependence of the device on the permissible values of its parameters. Based on the model built, parameters of a goniometer with a cell volume of 8 cm³ were determined; the maximum angular sensitivity of such a goniometer

with complete suppression of technical noise is $\delta\varphi_{sen}=1.0$ arcsec. The greatest contribution to the angle measurement error is from the instability of pumping power I_p ($\Delta I_p/I_p=0.05$) – 85 %, magnetic field B_0 ($\Delta B_0/B_0=10^{-8}$) – 13 %, temperature T ($\Delta T/T=0.1$) – 2 %.

The goniometer under consideration corresponds to the medium accuracy class, $\delta\varphi_{rot}\geq 10$ arcsec. It could be used in optical manufacturing for operational control, calibration, and certification of optical products. To improve the angular accuracy of the goniometer, it is necessary to increase the stability of the laser pumping intensity.

Keywords: goniometer, nuclear magnetic resonance, gas cell, optical pumping, Helmholtz coil, Larmor frequency.

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DEVELOPMENT OF METHODS FOR MONITORING AND OPTIMIZATION OF UNDERGROUND DRAINAGE SYSTEMS USING WIRELESS SENSOR NETWORKS AND ULTRA-WIDEBAND ANTENNAS (p. 26–36)

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This research focuses on optimizing ultra-wideband (UWB) antennas, which are critical in modern communication systems due to their wide frequency range (3.1–10.6 GHz) and high data transmission capabilities. The study addresses the challenge of optimizing key antenna parameters – such as return loss, peak gain, and radiation efficiency – while also ensuring energy efficiency and network longevity. Traditional optimization methods, such as LEACH-C, often fail to balance these factors, leading to suboptimal performance.

To solve this problem, the researchers developed the Generalized Position-based Optimization Neural Network (GPON) for UWB antenna optimization. They also evaluated the Position-based Hybrid Neural Network (PAN) method, comparing its performance with existing algorithms including LEACH-C, Firefly Algorithm (FA), HFAPSO, FA-ANN, and HWOABCA. The GPON model reduced return loss to 25.5 dB at 3.5 GHz and improved peak gain to 4.2 dB i, while maintaining 92 % radiation efficiency. In contrast, PAN demonstrated a 15–25 % improvement in residual energy and extended network lifetime by 20 % compared to LEACH-C.

These improvements were due to the integration of advanced neural network techniques in GPON and the effective use of positional data in PAN, enabling more precise and adaptive optimization. The ability to balance multiple performance metrics simultaneously – a challenge previous models struggled with – is a key feature. This balance is crucial for UWB antennas in communication systems where both performance and energy efficiency are vital. The findings are especially relevant for practical applications in wireless sensor networks, mobile communications, and radar systems, requiring long-term network reliability and optimal antenna performance.

Keywords: ultra-wideband, antenna optimization, GPON, energy efficiency, network longevity, neural networks.

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DEVELOPMENT MODEL OF A HIGH-PERFORMANCE MULTIPLE INPUT MULTIPLE OUTPUT MICROSTRIP ANTENNA BASED ON A PLANAR SERIES ARRAY WITH 842 ELEMENTS FOR 5G COMMUNICATION SYSTEMS (p. 37–49)

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MIMO (Multiple Input Multiple Output) makes a major contribution to 5G communication systems by increasing network capacity and spectrum efficiency. In 5G, MIMO enables the use of multiple antennas at base stations and user devices, allowing simultaneous sending and receiving of data over multiple paths. This significantly increases data throughput and connection reliability, especially in environments with high user density. In addition, MIMO technology supports the implementation

of beamforming, which focuses signals on a specific direction, reduces interference, and improves signal coverage and quality, making it one of the keys to achieving faster and more responsive 5G performance. Therefore, antennas with wide bandwidth, high gain and MIMO performance are crucial for supporting 5G communication systems. This paper proposes a high-performance MIMO microstrip antenna based on a series planar array with 8×2 elements operating at a resonant frequency of 3.5 GHz for 5G communication systems. A spiral stub and a feed inset are proposed to control the reflection coefficient and bandwidth of the antenna while the series planar array is proposed to increase the gain. To support the MIMO communication system, the proposed antenna is separated into two different ports with a certain distance. From the measurement results, the proposed antenna has high performance indicated by a wide bandwidth of 680 MHz (3–3.68 GHz) and a high gain of 17.8 dB at a resonant frequency of 3.5 GHz. In addition, the proposed antenna has high mutual coupling and diversity indicated by ECC and DG of 0.001 and 9.99 dB, respectively. This work provides a solution to design a high-performance microstrip antenna and can be implemented as a receiving antenna for 5G communication systems.

Keywords: microstrip antenna, high gain, MIMO system, planar array, 5G system.

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OPTIMIZATION OF DISTRIBUTED ACOUSTIC SENSORS BASED ON FIBER OPTIC TECHNOLOGIES (p. 50–59)

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This research investigates distributed acoustic sensors (DAS) based on fiber optic technologies, focusing on the impact of pressure on signal-to-noise ratio (SNR), noise levels, and dominant frequency shifts. DAS systems are widely used for infrastructure monitoring due to their ability to capture acoustic signals over long distances, making them ideal for seismic and pipeline monitoring.

The study examines how fluctuating pressure affects DAS performance, particularly signal quality and noise reduction. In applications like pipeline leak detection and seismic monitoring, pressure changes can degrade signal clarity and complicate anomaly detection. Understanding this relationship is key to optimizing DAS performance and improving system efficiency.

The experiment varied pressure from 0.1 atm to 5 atm, showing that increased pressure raised SNR from 10 dB to 48 dB, reduced noise from 10 dB to 7 dB, and shifted the dominant frequency from 0.5 Hz to 3 Hz. Fourier analysis provided insights into these frequency spectrum changes. Higher pressure compresses the medium, enhancing signal isolation and improving SNR while reducing noise. The frequency shift results from changes in acoustic wave propagation speed under higher pressure, highlighting its role in signal processing.

The key finding is that higher pressure significantly improves signal quality and reduces noise, enhancing DAS performance. The frequency shift improves environmental detection capabilities. These results are valuable for DAS applications in environments with pressure variations, like pipeline monitoring,

where high signal quality is crucial. Improved signal fidelity and frequency shifts make DAS systems more reliable for long-term monitoring and contribute to accurate anomaly detection.

Keywords: fiber optic technologies, distributed acoustic sensors, seismic monitoring, infrastructure monitoring.

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IDENTIFICATION OF CHARACTERISTICS OF CONCEPTUAL PROTOTYPE OF MICROPROCESSOR RESOURCE-SAVING RELAY PROTECTION SYSTEM (p. 60–69)

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The object of the study is the conceptual prototype of a microprocessor resource-saving relay protection system. Currently, relay protection ensures electrical networks reliable and efficient work, however, the traditional architecture is proprietary, not allowing to fix and replace damaged parts without a company specialist. Therefore, the open-architecture relay protection is a very pressing issue, but the problem lies in meeting the relay protection requirements. The data transmission protocols nRF and ESP-NOW, Hall sensors evaluation for AC current measurement determination and sensor accuracy improvement was implemented. Experimental validation demonstrated that nRF and ESP-NOW protocols meet the delay and reliability requirements, however, the nRF protocol is more suitable due to its flexibility and obstacle penetration. The data demonstrated that the most effective conditions are without obstacles at 15 meters from the modem and with obstacles 5 meters from the modem. The experiment of Hall sensors characteristics determination

demonstrated the accuracy of current measurement with the set values of the opening and closing currents. Nevertheless, it is not accurate (12.45 %) for the relay protection application. Therefore, the application of the changing values of the opening and closing currents is more effective and accuracy reaches 6.92 %. As a result, the service life of the Hall sensor was determined, and even after 10 million openings, the open state time remained unchanged. Therefore, the approximation function for current amplitude determination depending on open state time was found. On the other hand, Hall sensors may suffer from temperature drift and require further optimization to be fully reliable. The study limitation is the current range from 0 to 800 A.

Keywords: relay protection, reed switch, Hall sensor, magnetic field, open architecture.

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DEVELOPMENT OF MATHEMATICAL MODELS OF HEAT CONDUCTIVITY FOR MODERN ELECTRONIC DEVICES WITH ELEMENTS CONTAINING FOREIGN INCLUSIONS (p. 70–79)

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This paper considers the heat conduction process for an isotropic medium containing a foreign half-through inclusion and heated by a locally concentrated heat flow. Linear and non-linear mathematical models for determining the temperature field have been built to establish the temperature regimes for the effective operation of electronic devices. The coefficient of thermal conductivity of a non-uniform structure is represented as a whole, using asymmetric unit functions, which automatically provides the conditions of ideal thermal contact on the surfaces of materials. This results in solving one heat conduction equation with discontinuous and singular coefficients. A linearizing function was introduced to linearize the nonlinear boundary value problem. Analytical-numerical solutions

of linear and nonlinear boundary-value problems have been obtained in a closed form. A linear temperature dependence of the coefficient of thermal conductivity of structural materials was chosen for a heat-sensitive medium. As a result, an analytical-numerical solution was derived, which determines the temperature distribution in this medium. On this basis, a numerical experiment was performed, the results of which are graphically displayed and confirm the adequacy of the constructed mathematical models to a real physical process.

The materials of the plate and inclusion are silicon and silver. The results for these materials based on the linear and non-linear model differ by 7%. Their slight difference is explained by the fact that the values of the temperature coefficient of thermal conductivity are small. The models built make it possible to analyze the given environments in terms of their thermal resistance. As a result, it becomes possible to improve it, and protect structures from overheating, which could lead to the failure of individual nodes and their elements and the entire electronic device.

Keywords: thermal resistance of the structure, foreign half-through inclusion, ideal thermal contact, convective heat exchange.

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DEVISING A METHOD FOR DETERMINING THE MOISTURE CONDUCTIVITY COEFFICIENT OF SUBGRADE SOILS TAKING INTO ACCOUNT EUROPEAN APPROACHES AND STANDARDS (p. 80–89)

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The object of this study is the theoretical and methodological approaches to determining the coefficient of moisture conductivity of subgrade soils. The work focuses on considering the European approaches and standards when devising a method for determining the coefficient of moisture conductivity of soils.

In the course of the research, a method was developed for determining the coefficient of moisture conductivity of soils K_1 , which characterizes the diffusion movement of water, through the filtration coefficient K_0 , calculated in accordance with European requirements based on laboratory test data.

The proposed method is based on a mathematical model built on the basis of the differential equation of changes in soil moisture. The model is special in that, unlike existing ones, the movement of water was modeled from the bottom up, which reflects the process of moisture accumulation in the lower layers of the subgrade from groundwater or topwater.

A good agreement of the mathematical model with the data by other authors was obtained (the relative error did not exceed 12.98 %).

A direct relationship between the moisture conductivity coefficient of soils K_1 and their initial moisture content W_0 and an inverse relationship between K_1 and the total moisture capacity of soils W_{FH} were established in the paper. Dependences were derived in the range of changes in initial soil moisture W_0 from 0.08 to 0.15 and W_{FH} from 0.15 to 0.5. It was found that the values of the moisture conductivity coefficient of soils K_1 increase from $4.64 \cdot 10^{-6}$ to $3.81 \cdot 10^{-5}$ m²/h with an increase in their initial moisture content and with a decrease in total moisture capacity.

From the point of view of engineering practice of road construction, the proposed method makes it possible to predict seasonal changes in soil moisture in the subgrade, to determine the strength of the road structure. This makes it possible to make sound design decisions on the installation of drainage systems on roads in order to extend their service life.

Keywords: soil moisture, coefficient of soil moisture conductivity, subgrade, road structure.

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DETERMINING WORKING CHARACTERISTICS OF THE EXCESS AIR PRESSURE SYSTEM IN AN EMERGENCY HATCH BASED ON JET WATER-GAS EJECTORS (p. 90–99)

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The object of this study is jet water and gas ejectors in the fire safety system of ships. The problem solved relates to the fact that in the event of a fire in the area of the exit from the ship's emergency room, the heat energy increases dangerously and a large amount of smoke spreads throughout the ship's rooms. These factors require immediate sealing of the emergency room, which limits the immediate access of emergency teams to the room. Installation of a local excess air pressure system in the emergency hatch on the basis of jet water and gas ejectors could make it possible to shield thermal energy and localize smoke gases in the emergency room without sealing it to ensure prompt access of emergency teams to it. The following results were achieved – the adequacy of theoretical studies of the processes of localization of flue gases in the emergency room without its sealing was confirmed by the experimental method. The investigated problem was solved by optimizing processes: the rate of change in the natural indicator of the weakening of environment during the start-up of the local excess air pressure system in the emergency hatch based on jet water and gas ejectors; the effectiveness of reducing the temperature of heated gases in the superstructure during the operation of the excess air pressure system in the

emergency hatch based on jet water-gas ejectors. Special feature of the results was the formation of an air curtain obtained by the selection of a part of high-temperature flue gases in the housings of jet water-gas ejectors, their heat-mass exchange processing and output back into the flow. This created conditions under which thermal energy is shielded with an efficiency of 85–88 %. The scope and conditions of practical use of the results are shipbuilding and ship fire safety design.

Keywords: water-gas jet ejector, emergency hatch, natural attenuation index, thermal energy.

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ОПТИМІЗАЦІЯ СОНЯЧНОГО ЕЛЕМЕНТА НА ОСНОВІ ТЕЛУРИДУ КАДМІЮ ШЛЯХОМ ВНЕСЕННЯ ПОГЛИНАЮЧОГО ШАРУ CdSeTe (МОДЕЛЮВАННЯ ГЕТЕРОСТРУКТУРИ) (с. 6–12)

Г. А. Льчук, І. В. Семків, М. С. Каркульовська, В. М. Ващинський, М. В. Соловійов

Сонячні елементи на основі телуриду кадмію є одними із найпоширеніших пристроїв для фотоелектричних застосувань. Однак ефективність перетворення енергії цих елементів залишається недостатньо високою. Використовуючи програмне середовище SCAPS проведено дослідження та оптимізацію класичного тонкоплівкового сонячного елемента на основі CdTe. Структура цього елемента складалася з ГТО в якості прозорого провідного контакту, шару сульфиду кадмію (CdS) і шару поглинача телуриду кадмію (CdTe) з металевим контактом. Для оптимізації такої конструкції з точки зору ефективності перетворення потужності, розглянуто вплив товщини та концентрації домішок акцепторів в поглинаючому шарі CdTe, а також вплив товщини та концентрації домішок донорів в буферному CdS шарі. Встановлено, що оптимальні товщини для буферного шару CdS та поглинаючого CdTe шарів відповідно становлять 50 нм та 3000 нм. Як один із варіантів оптимізації для покращення ефективності пристрою запропоновано ввести додатковий шар CdSeTe між шарами CdS та CdTe. Проаналізовано основні фотовольтаїчні параметри такого сонячного елемента в залежності від товщини шару CdSeTe та вмісту в ньому селену. Продемонстровано, що додавання твердого розчину CdSeTe в шар поглинача CdTe товщиною 1500 нм підвищує ефективність сонячного елемента на 6,84 %. Проведено порівняння основних фотовольтаїчних характеристик сонячних елементів CdS/CdTe та CdS/CdSeTe/CdTe. Отримані результати показали, що змодельована структура CdS/CdSeTe/CdTe забезпечує кращу ефективність фотоперетворення у світловому спектрі AM1.5G в порівнянні з класичною CdS/CdTe структурою. Такі елементи можуть використовуватися для формування високоефективних сонячних панелей.

Ключові слова: сонячний елемент, SCAPS, тонкі плівки, гетероструктури, телурид кадмію, халькогенід кадмію.

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ОЦІНКА ПОТЕНЦІЙНОЇ ТОЧНОСТІ МАЛОГАБАРИТНОГО ГОНІОМЕТРА ІЗ РОЗШИРЕНИМ ДИНАМІЧНИМ ДІАПАЗОНОМ НА ОСНОВІ ЯДЕРНОГО МАГНІТНОГО РЕЗОНАНСУ (с. 13–25)

С. В. Іванов

Дослідження присвячено оцінці потенційних точнісних характеристик малогабаритного гоніометра на основі ядерного магнітного резонансу з розширеним динамічним діапазоном. Це потребувало отримання моделі похибок гоніометра, оцінки його точності на основі цієї моделі та формулювання практичних рекомендацій з розробки такого приладу на основі виконаної оцінки точності.

Для проведення оцінки точності ядерного гоніометра розроблено теоретичну модель, яка дозволяє визначити оптимальні робочі параметри газової суміші комірки, діапазони їх допустимих змін, чутливість гоніометра, залежність його характеристик від зовнішніх і внутрішніх факторів. Зокрема, визначено залежність вихідного сигналу приладу від параметрів газової суміші, оптичної накачки. Для гоніометра з коміркою об'ємом 8 см³ оптимальна температура складає 130 °С, оптимальна інтенсивність випромінювання накачки 5 мВт.

Також визначено залежність вихідного сигналу від вимірюваного кута повороту, проаналізовано шуми та залежність похибки приладу за допустимими значеннями його параметрів. На основі розробленої моделі визначено параметри гоніометра з коміркою об'ємом 8 см³; гранична кутова чутливість такого гоніометра при повному придушенні технічних шумів складає $\delta\varphi_{sen}=1.0$ кут.сек. Найбільший вклад в похибку вимірювання кута вносить нестабільність потужності накачки I_p ($\Delta I_p/I_p=0,05$) – 85 %; магнітного поля B_0 ($\Delta B_0/B_0=10^{-8}$) – 13 %, температури T ($\Delta T/T=0,1$) – 2 %.

Розглянутий гоніометр відповідає середньому класу точності, $\delta\varphi_{tot}\geq 10$ кут.сек. Він може знайти застосування в оптичному виробництві для оперативного контролю, атестації та паспортизації оптичних виробів. Для поліпшення кутової точності гоніометра потрібно підвищувати стабільність інтенсивності лазерного накачування.

Ключові слова: гоніометр, ядерний магнітний резонанс, газова комірка, оптичне накачування, котушка Гельмгольца, Ларморова частота.

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РОЗРОБКА МЕТОДІВ МОНІТОРИНГУ ТА ОПТИМІЗАЦІЇ ПІДЗЕМНИХ ДРЕНАЖНИХ СИСТЕМ З ВИКОРИСТАННЯМ БЕЗДРОТОВИХ СЕНСОРНИХ МЕРЕЖ ТА УЛЬТРАШИРОКОСМУГОВИХ АНТЕН (с. 26–36)

Kabi Yelikbay, Pramod Kumar, Ruslan Kassym, Tansaule Serikov, Maxsat Orunbekov, Ainur Turdy, Marzhan Temirbekova, Arai Tolegenova, Akmaral Tlenshieva, Makbal Kassymova

Це дослідження зосереджено на оптимізації ультраширококутєвих (УШС) антен, які є критично важливими в сучасних системах зв'язку завдяки їх широкому діапазону частот (3,1–10,6 ГГц) і високим можливостям передачі даних. У дослідженні розглядається

ся проблема оптимізації ключових параметрів антени, таких як зворотні втрати, пікове посилення та ефективність випромінювання, а також забезпечення енергоефективності та довговічності мережі. Традиційні методи оптимізації, такі як LEACH-C, часто не в змозі збалансувати ці фактори, що призводить до неоптимальної продуктивності.

Щоб вирішити цю проблему, було розроблено нейромережу Generalized Position-based Optimization Neural Network (GPON) для оптимізації УШС антени. Здійснено оцінку методу гібридної нейронної мережі на основі позиції (ПНМ), порівнявши його продуктивність з існуючими алгоритмами, включаючи LEACH-C, алгоритм Firefly, HFAPSO, FA-ANN і HWOABCA. Модель GPON зменшила зворотні втрати до 25,5 дБ на 3,5 ГГц і покращила пікове посилення до 4,2 дБ і, зберігаючи ефективність випромінювання на 92 %. Навпаки, PAN продемонстрував покращення залишкової енергії на 15–25 % і подовжив термін служби мережі на 20 % порівняно з LEACH-C.

Ці вдосконалення відбулися завдяки інтеграції передових методів нейронної мережі в GPON і ефективному використанню позиційних даних у ПНМ, що забезпечує більш точну та адаптивну оптимізацію. Здатність збалансувати декілька показників продуктивності одночасно – це проблема, з якою боролися попередні моделі – є ключовою особливістю. Цей баланс має вирішальне значення для УШС антен у системах зв'язку, де продуктивність та енергоефективність є життєво важливими. Висновки особливо актуальні для практичних застосувань у бездротових сенсорних мережах, мобільному зв'язку та радарних системах, що вимагають довгострокової надійності мережі та оптимальної продуктивності антени.

Ключові слова: ультраширокий діапазон, оптимізація антени, GPON, енергоефективність, довговічність мережі, нейронні мережі.

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МОДЕЛЬ РОЗРОБКИ ВИСОКОЕФЕКТИВНОЇ МІКРОСМУЖКОВОЇ АНТЕНИ МІМО НА ОСНОВІ ПЛОСКОЇ ПОСЛІДОВНОЇ РЕШІТКИ З 8Ч2 ЕЛЕМЕНТАМИ ДЛЯ СИСТЕМ ЗВ'ЯЗКУ 5G (с. 37–49)

Syah Alam, Indra Surjati, Lydia Sari, Yuli Kurnia Ningsih, Suryadi, Teguh Firmansyah, Zahriladha Zakaria

Технологія МІМО (Multiple Input Multiple Output) здійснює значний внесок у розвиток систем зв'язку 5G зі збільшенням пропускної здатності мережі та ефективності використання спектру. У системах 5G технологія МІМО дозволяє використовувати кілька антен на базових станціях і пристроях користувачів, забезпечуючи одночасну відправку та прийом даних по декількох каналах. Це дозволяє значно підвищити пропускну здатність і надійність з'єднання, особливо у середовищах з високою щільністю користувачів. Крім того, технологія МІМО підтримує реалізацію технології формування діаграми спрямованості, яка фокусує сигнали в певному напрямку, знижує перешкоди й покращує покриття та якість сигналу, що робить її одним з ключових факторів для підвищення швидкодії та відгуку систем 5G. Таким чином, антени з широкою смугою пропускання, високим коефіцієнтом посилення та ефективністю МІМО мають вирішальне значення для підтримки систем зв'язку 5G. У даній роботі пропонується високоефективна мікросмужкова антена МІМО на основі послідовної плоскої решітки з 8×2 елементами, що працює на резонансній частоті 3,5 ГГц для систем зв'язку 5G. Для регулювання коефіцієнта відбиття та смуги пропускання антени пропонується використовувати спіральний шлейф і фідерну вставку, а для збільшення коефіцієнта посилення – послідовну плоску решітку. Для підтримки системи зв'язку МІМО запропонована антена розділена на два різних порти на певній відстані. Виходячи з результатів вимірювань, запропонована антена має високу ефективність, про що свідчить широка смуга пропускання 680 МГц (3–3,68 ГГц) та високий коефіцієнт посилення 17,8 дБ за резонансної частоти 3,5 ГГц. Крім того, запропонована антена має високий взаємний зв'язок і рознесення, про що свідчать значення ECC і DG, які становлять 0,001 і 9,99 дБ відповідно. Дана робота представляє рішення для проектування високоефективної мікросмужкової антени, що може бути реалізована в якості приймальної антени для систем зв'язку 5G.

Ключові слова: мікросмужкова антена, високий коефіцієнт посилення, система МІМО, плоска антенна решітка, система 5G.

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ОПТИМІЗАЦІЯ РОЗПОДІЛЕНИХ АКУСТИЧНИХ ДАТЧИКІВ НА ОСНОВІ ВОЛОКОННО-ОПТИЧНИХ ТЕХНОЛОГІЙ (с. 50–59)

Askar Abdykadyrov, Nurzhigit Smailov, Akezhan Sabibolda, Gulzhaina Tolen*, Zhandos Dosbayev, Zhomart Ualiyev, Rashida Kadyrova

Це дослідження досліджує розподілені акустичні датчики (РАД), засновані на волоконно-оптичних технологіях, зосереджуючись на впливі тиску на відношення сигнал/шум (ВСШ), рівні шуму та домінуючі зрушення частоти. Системи РАД широко використовуються для моніторингу інфраструктури завдяки своїй здатності фіксувати акустичні сигнали на великих відстанях, що робить їх ідеальними для сейсмічного моніторингу та моніторингу трубопроводів.

Дослідження вивчає, як коливання тиску впливає на продуктивність РАД, зокрема на якість сигналу та зменшення шуму. У таких програмах, як виявлення витоків у трубопроводі та сейсмічний моніторинг, зміни тиску можуть погіршити чіткість сигналу та ускладнити виявлення аномалій. Розуміння цього зв'язку є ключовим для оптимізації продуктивності РАД і підвищення ефективності системи.

Експеримент змінював тиск від 0,1 атм до 5 атм, показуючи, що підвищення тиску підвищило ВСШ з 10 дБ до 48 дБ, зменшило шум з 10 дБ до 7 дБ і зрушило домінуючу частоту з 0,5 Гц до 3 Гц. Аналіз Фур'є дав зрозуміти ці зміни частотного спектру. Більш високий тиск стискає середовище, покращуючи ізоляцію сигналу та покращуючи ВСШ, одночасно зменшуючи шум. Зсув частоти є результатом зміни швидкості поширення акустичної хвилі під високим тиском, підкреслюючи його роль в обробці сигналу.

Ключовий висновок полягає в тому, що вищий тиск значно покращує якість сигналу та зменшує шум, покращуючи продуктивність РАД. Зсув частоти покращує можливості виявлення навколишнього середовища. Ці результати є цінними для додатків РАД у

середовищах із коливаннями тиску, як-от моніторинг трубопроводів, де висока якість сигналу має вирішальне значення. Покращена точність сигналу та зрушення частоти роблять системи РАД більш надійними для тривалого моніторингу та сприяють точному виявленню аномалій.

Ключові слова: волоконно-оптичні технології, розподілені акустичні датчики, сейсмічний моніторинг, моніторинг інфраструктури.

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ВИЗНАЧЕННЯ ХАРАКТЕРИСТИК КОНЦЕПТУАЛЬНОГО ПРОТОТИПУ МІКРОПРОЦЕСОРНОЇ РЕСУРСОЗБЕРІГАЮЧОЇ СИСТЕМИ РЕЛЕЙНОГО ЗАХИСТУ (с. 60–69)

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Об'єктом дослідження є концептуальний прототип мікропроцесорної ресурсозберігаючої системи релейного захисту. В даний час релейний захист забезпечує надійну й ефективну роботу електромереж, проте традиційна архітектура є запатентованою, що не дозволяє проводити ремонт та заміну пошкоджених деталей без участі фахівця компанії. Тому релейний захист із відкритою архітектурою є досить актуальним питанням, проте проблема полягає в дотриманні вимог до релейного захисту. Проведено оцінку протоколів передачі даних nRF та ESP-NOW, датчиків Холла для вимірювання величини змінного струму й підвищення точності датчиків. Експериментальна перевірка показала, що протоколи nRF та ESP-NOW відповідають вимогам щодо затримки та надійності, проте протокол nRF є більш підходящим завдяки своїй гнучкості та здатності подолати перешкод. Отримані дані показали, що найбільш ефективними умовами є відсутність перешкод на відстані 15 метрів від модему та наявність перешкод на відстані 5 метрів від модему. Експеримент з визначення характеристик датчиків Холла показав точність вимірювання струму при заданих значеннях струмів розмикання й замикання. Однак він не є точним (12,45 %) для застосування в релейному захисті. Тож застосування змінних значень струмів розмикання й замикання є більш ефективним, а точність досягає 6,92 %. В результаті було визначено термін служби датчика Холла, і навіть після 10 мільйонів розмикань час перебування в розімкнутому стані залишався незмінним. Таким чином, була знайдена апроксимуюча функція для визначення амплітуди струму в залежності від часу перебування в розімкнутому стані. З іншого боку, датчики Холла можуть страждати від температурного дрейфу й вимагають подальшої оптимізації для забезпечення повної надійності. Обмеженням дослідження є діапазон струму від 0 до 800 А.

Ключові слова: релейний захист, геркон, датчик Холла, магнітне поле, відкрита архітектура.

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РОЗРОБЛЕННЯ МАТЕМАТИЧНИХ МОДЕЛЕЙ ТЕПЛОПРОВІДНОСТІ ДЛЯ ЕЛЕМЕНТІВ ПРИСТРОЇВ З ВКЛЮЧЕННЯМИ (с. 70–79)

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Розглянуто процес теплопровідності для ізотропного середовища, що містить чужорідне напівнаскрізне включення, та нагрівається локально зосередженим тепловим потоком. Для встановлення температурних режимів ефективної роботи електронних пристроїв розроблено лінійну і нелінійну математичні моделі визначення температурного поля. Коефіцієнт теплопровідності неоднорідної конструкції подано як ціле, з використанням асиметричних одиничних функцій, що автоматично забезпечує умови ідеального теплового контакту на поверхнях стику матеріалів. Це приводить до розв'язування одного рівняння теплопровідності з розривними та сингулярними коефіцієнтами. Для лінеаризації нелінійної крайової задачі запроваджено лінеаризуючу функції. У замкнутому вигляді отримано аналітично-числові розв'язки лінійної і нелінійної крайових задач. Для термочутливого середовища вибрано лінійну температурну залежність коефіцієнта теплопровідності конструкційних матеріалів. У результаті отримано аналітично-числовий розв'язок, який визначає розподіл температури у цьому середовищі. На цій основі виконано числовий експеримент, результати якого графічно відображені та підтверджують адекватність розроблених математичних моделей реальному фізичному процесу.

Матеріалом пластини та включення виступають кремній та срібло. Отримані результати для цих матеріалів за лінійною і нелінійною моделлю відрізняються на 7 %. Незначна їх відмінність пояснюється тим, що значення температурного коефіцієнта теплопровідності є невеликими. Розроблені моделі дають змогу аналізувати наведені середовища щодо їх термостійкості. Унаслідок, стає можливим її підвищити, а конструкції захистити від перегрівання, яке може привести до виходу з ладу окремих вузлів та їх елементів і цілого електронного пристрою.

Ключові слова: термостійкість конструкції, чужорідне напівнаскрізне включення, ідеальний тепловий контакт, конвективний теплообмін.

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РОЗРОБЛЕННЯ МЕТОДУ ВИЗНАЧЕННЯ КОЕФІЦІЄНТА ВОЛОГОПРОВІДНОСТІ ҐРУНТІВ ЗЕМЛЯНОГО ПОЛОТНА З УРАХУВАННЯМ ЄВРОПЕЙСЬКИХ ПІДХОДІВ І СТАНДАРТІВ (с. 80–89)

А. В. Бубела, Л. П. Бондаренко, Є. І. Кватадзе, В. В. Стьожка, А. В. Івко

Об'єктом досліджень є теоретико-методичні підходи до визначення коефіцієнта вологопровідності ґрунтів земляного полотна. Основний фокус роботи спрямований на врахування європейських підходів і стандартів при розробленні методу визначення коефіцієнта вологопровідності ґрунтів.

У ході досліджень розроблено метод визначення коефіцієнта вологопровідності ґрунтів K_1 , що характеризує дифузійний рух води, через фільтраційний коефіцієнт K_0 , розрахований відповідно до європейських вимог за даними лабораторних випробувань.

Запропонований метод базується на математичній моделі, отриманій на основі диференціального рівняння зміни вологості в ґрунті. Модель особлива тим, що на відміну від існуючих, рух води моделювався знизу вгору, що відображає процес вологонакопичення в нижніх шарах земляного полотна від ґрунтових вод або верховодки.

Отримано гарне узгодження математичної моделі з даними інших авторів (відносна похибка не перевищила 12.98 %).

В роботі отримано пряму залежність між коефіцієнтом вологопровідності ґрунтів K_1 і їх початковою вологістю W_0 та обернену залежність між K_1 і повною вологоємністю ґрунтів $W_{ПВ}$. Залежності отримано в діапазоні зміни початкової вологості ґрунту W_0 від 0.08 до 0.15 та $W_{ПВ}$ від 0.15 до 0.5. Встановлено, що значення коефіцієнта вологопровідності ґрунтів K_1 збільшуються від $4,64 \cdot 10^{-6}$ до $3,81 \cdot 10^{-5}$ м²/год при збільшенні їх початкової вологості та при зменшенні повної вологоємності.

З точки зору інженерної практики дорожнього будівництва, запропонований метод дає можливість прогнозувати сезонні зміни вологості ґрунтів земляного полотна, визначати міцність дорожньої конструкції. Це дозволяє приймати обґрунтовані проектні рішення щодо влаштування дренажних систем на автошляхах задля подовження строку їх експлуатації.

Ключові слова: вологість ґрунту, коефіцієнт вологопровідності ґрунту, земляне полотно, дорожня конструкція.

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ВИЗНАЧЕННЯ РОБОЧИХ ХАРАКТЕРИСТИК СИСТЕМИ ПІДПОРУ ПОВІТРЯ В АВАРІЙНОМУ ЛЮКУ НА БАЗІ СТРУМИННИХ ВОДОГАЗОВИХ ЕЖЕКТОРІВ (с. 90–99)

С. О. Гринчак

Об'єктом досліджень є струминні водогазові ежектори в системі забезпечення протипожежної безпеки кораблів. Проблема, що вирішувалася, – при пожежі в районі виходу з аварійного приміщення судна небезпечно підвищується теплова енергія і велика кількість диму поширюється по приміщеннях судна. Ці чинники вимагають негайної герметизації аварійного приміщення, що обмежує оперативний доступ аварійних команд в приміщення. Встановлення системи місцевого підпору повітря в аварійному люку на базі струминних водогазових ежекторів дозволить екранувати теплову енергію і локалізувати димові гази в аварійному приміщенні без його герметизації для забезпечення оперативного доступу аварійних команд до нього. Досягнуті наступні основні результати – підтверджено експериментальним методом адекватність теоретичних досліджень процесів локалізації димових газів в аварійному приміщенні без його герметизації. Досліджувана проблема була вирішена шляхом оптимізації процесів: швидкості зміни натурального показника послаблення середовища під час запуску місцевої системи підпору повітря в аварійному люку на базі струминних водогазових ежекторів; ефективності зниження температури нагрітих газів в надбудові при роботі системи підпору повітря в аварійному люку на базі струминних водогазових ежекторів. Особливістю отриманих результатів стало формування повітряної завіси, отриманої шляхом відбору частини високотемпературних димових газів у корпуси струминних водогазових ежекторів, їх тепломасообмінної обробки та виводу назад у потік. Це створило умови, при яких екранування теплової енергії відбувається з ефективністю 85–88 %. Сфера та умови практичного використання отримані результатів – суднобудування та проектування протипожежної суднової безпеки.

Ключові слова: водогазовий струминний ежектор, аварійний люк, натуральний показник послаблення середовища, теплова енергія.

MIMO (Multiple Input Multiple Output) makes a major contribution to 5G communication systems by increasing network capacity and spectrum efficiency. In 5G, MIMO enables the use of multiple antennas at base stations and user devices, allowing simultaneous sending and receiving of data over multiple paths. This significantly increases data throughput and connection reliability, especially in environments with high user density. In addition, MIMO technology supports the implementation of beamforming, which focuses signals on a specific direction, reduces interference, and improves signal coverage and quality, making it one of the keys to achieving faster and more responsive 5G performance. Therefore, antennas with wide bandwidth, high gain and MIMO performance are crucial for supporting 5G communication systems. This paper proposes a high-performance MIMO microstrip antenna based on a series planar array with 8×2 elements operating at a resonant frequency of 3.5 GHz for 5G communication systems. A spiral stub and a feed inset are proposed to control the reflection coefficient and bandwidth of the antenna while the series planar array is proposed to increase the gain. To support the MIMO communication system, the proposed antenna is separated into two different ports with a certain distance. From the measurement results, the proposed antenna has high performance indicated by a wide bandwidth of 680 MHz (3–3.68 GHz) and a high gain of 17.8 dB at a resonant frequency of 3.5 GHz. In addition, the proposed antenna has high mutual coupling and diversity indicated by ECC and DG of 0.001 and 9.99 dB, respectively. This work provides a solution to design a high-performance microstrip antenna and can be implemented as a receiving antenna for 5G communication systems

Keywords: microstrip antenna, high gain, MIMO system, planar array, 5G system

DEVELOPMENT MODEL OF A HIGH-PERFORMANCE MULTIPLE INPUT MULTIPLE OUTPUT MICROSTRIP ANTENNA BASED ON A PLANAR SERIES ARRAY WITH 8×2 ELEMENTS FOR 5G COMMUNICATION SYSTEMS

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1. Introduction

5G communication systems require more sophisticated and diverse antennas than previous generations to support various technological advancements, such as MIMO and millimeter wave (mmWave) [1–3]. MIMO (Multiple Input Multiple Output) is a technology that plays a key role in 5G communication systems. The main advantage of MIMO in 5G is its ability to significantly increase capacity and data rates without requiring more frequency spectrum. By using

multiple antennas on the transmit and receive side, MIMO allows simultaneous data transmission over multiple paths, reducing interference and increasing spectral efficiency [4, 5]. In addition, MIMO can improve signal coverage and reliability by using techniques such as beamforming, which focuses the signal toward a specific user. This is especially important in delivering a faster and more stable experience for users in sub-urban areas [6]. According to [7], the resonant frequency for 5G communication systems is categorized into three bands: high, middle, and low. One of the recommended

frequencies for 5G communication systems is 3.5 GHz, which is included in the middle band category and dynamic environments, such as urban or high-mobility areas [8].

Furthermore, microstrip antennas offer several important advantages for 5G applications, particularly in terms of integration, size, and performance [9, 10]. Due to their thin and lightweight design, microstrip antennas can be easily integrated into portable devices such as smartphones and IoT devices, as well as into network infrastructure such as base stations [11, 12]. They can also be manufactured in arrays, enabling the implementation of MIMO and beamforming technologies, which are essential for increasing the capacity and transmission speed in 5G networks [13, 14]. In addition, microstrip antennas can be designed to operate at a wide range of frequencies, including high frequencies such as mmWave used in 5G, while maintaining good efficiency. Their relatively low production costs and ability to be printed on a variety of substrates also make them an economical and practical choice for widespread 5G deployment. However, microstrip antennas have certain drawbacks, such as narrow bandwidth, low gain, and limited directivity. The primary parameters that indicate an antenna's performance include the reflection coefficient, bandwidth, gain, and radiation pattern. Therefore, antennas with wide bandwidth and high gain are crucial for supporting wireless communication systems such as Wi-Fi, 4G, and 5G. Moreover, high-performance antennas with multiple input multiple output are essential to facilitate communication between the transmitter and receiver, especially for 5G communication systems.

2. Literature review and problem statement

Several previous studies have explored and proposed microstrip antennas for 5G communication systems using various techniques, including fractal designs, arrays, and parasitic elements. Furthermore, in a study presented by [10], microstrip antennas with wider bandwidths were achieved by incorporating parasitic elements placed above the radiating elements. However, the antenna's gain remained low, necessitating further improvement. Previous work [15] proposed a fractal antenna for 5G communication with MIMO configuration operating at a resonant frequency of 3.5 GHz. However, the gain of the proposed antenna is still low at about 3 dB. Another work [16] proposed a ten-element MIMO array antenna that operates at a resonant frequency of 3.5 GHz. However, the bandwidth of the proposed antenna is still low at about 200 MHz. Moreover, the previous work [17] presented a wideband microstrip antenna operating at a resonant frequency of 3.35–3.95 GHz with a 2×2 element MIMO array. However, the gain of the proposed antenna is only 12.6 dB. Another study by [18] proposed a microstrip antenna array with four elements operating at a resonant frequency of 3.5 GHz, achieving a bandwidth of 0.7 GHz and a gain of 9.24 dB. Nevertheless, the increase in bandwidth was accompanied by a decrease in gain, indicating an inverse relationship between bandwidth and gain. In addition, previous work by [19] proposed a microstrip antenna using an array with 4×2 elements with a bandwidth of 0.6 GHz and a gain of 12.2 dB. However, the proposed antenna does not support MIMO communication systems. Other findings describe MIMO microstrip antennas based on vertical and horizontal configurations with 2 ports operating at resonant frequencies of 3.5 GHz and 6 GHz [20].

However, the gain obtained is still low at around 7.8 dB. Based on the literature review [15–20], the limitation of previous works is that the proposed antenna still has low gain, narrow bandwidth and does not support MIMO. Therefore, an antenna with wide bandwidth, high gain and MIMO support is needed as a solution for receivers in 5G communication systems. In addition, MIMO technology supports the implementation of beamforming, which focuses signals on a specific direction, reduces interference, and improves signal coverage and quality, making it one of the keys to achieving faster and more responsive 5G performance.

3. The aim and objectives of the study

The aim of the study is to propose an antenna configured with two different ports separated by a certain distance in order to support MIMO capabilities.

To achieve this aim, the following objectives are accomplished:

- to produce a design and model of a microstrip antenna that operates at a resonance frequency of 3.5 GHz with a bandwidth of 200 MHz for a 5G communication system;
- to produce a design and model of a microstrip antenna with a high gain ≥ 12 dB that operates at a frequency of 3.5 GHz for a 5G communication system;
- to validate and measure microstrip antennas that can be used in MIMO communication systems with low mutual coupling $S_{21} \leq -20$ dB.

4. Materials and methods

The object of the study is 5G communication systems. The main hypothesis of the study is as follows. A high-performance MIMO microstrip antenna based on a series planar array with 8×2 elements operating at a resonant frequency of 3.5 GHz; will improve the capabilities of 5G communication systems.

The proposed antenna is designed using an FR-4 substrate with a dielectric constant of 4.3, tan delta of 0.0265 and thickness of 1.6 mm. The radiation element of the antenna is represented by a rectangular patch placed on the top layer of the substrate while the bottom layer functions as a ground plane. The antenna is connected directly with a brass connector using a microstrip line with an impedance of 50 ohms. The evolution and models of the proposed antenna are shown in Fig. 1. The antenna is designed and simulated using EM simulation based on HFSS 15.0.

Fig. 1 shows that the proposed antenna is developed in six models. Model 1 proposes an antenna with a single element that operates at a resonance frequency of 3.5 GHz, which is represented in Fig. 1, *a*. Furthermore, model 2 and model 3 propose two-element and four-element array antennas based on a series configuration with a spiral stub shown in Fig. 1, *b*, *c*.

Model 4 proposes an eight-element array antenna by adding an inset fed to the antenna patch while model 5 proposes an array antenna with 8×2 elements configured based on the horizontal planar shown in Fig. 1, *d*, *e*. The last model proposes an array antenna with 8×2 elements configured as MIMO using two ports separated by a certain distance represented by Fig. 1, *f*. The addition of the spiral stub and fed inset aims to reduce the reflection coefficient while adding the number of elements on the array antenna aims to increase the gain.

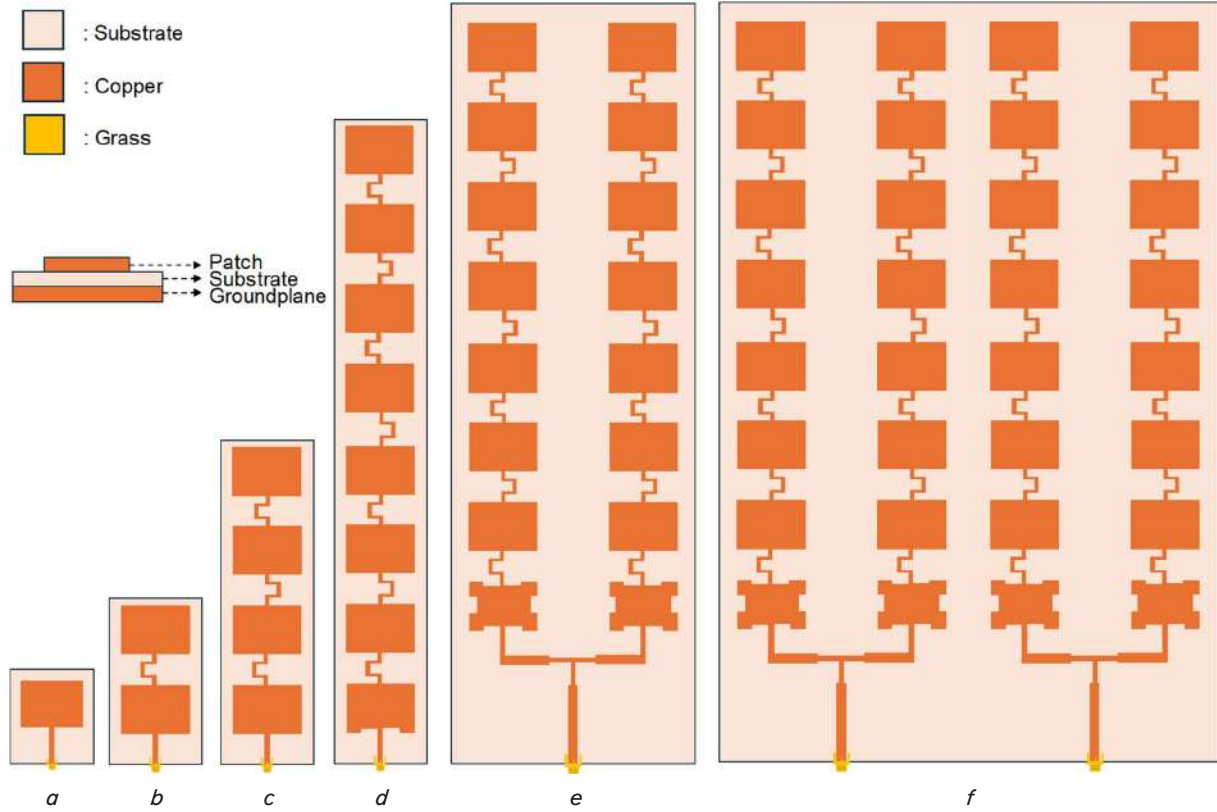


Fig. 1. Evolution of the proposed antenna: *a* – single-element; *b* – 2-element array; *c* – 4-element array; *d* – 8-element array; *e* – 8×2 element planar array; *f* – MIMO planar array

5. Results of the design and realization of the proposed antenna

5.1. Design of a series array antenna

At the first stage, the antenna is designed with a rectangular patch to operate at a resonant frequency of 3.5 GHz. The length and width of the antenna patch are represented respectively by W_p and L_p , which are determined based on the following equation [21]:

$$W_p = \frac{c}{2f_o\sqrt{\epsilon_r}}, \tag{1}$$

$$L_p = L_{eff} - \Delta_L, \tag{2}$$

$$L_{eff} = \frac{c}{2f_o\sqrt{\epsilon_{eff}}}, \tag{3}$$

$$\epsilon_{eff} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[1 + 12 \frac{h}{W} \right]^{-\frac{1}{2}}, \tag{4}$$

$$\Delta_L = 0.412 \frac{(\epsilon_{eff} + 0.3) \left(\frac{W}{h} + 0.264 \right)}{(\epsilon_{eff} - 0.258) \left(\frac{W}{h} + 0.8 \right)}. \tag{5}$$

In this context, W_p and L_p denote the width and length of the patch, respectively; f_o signifies the resonance frequency, ϵ_r indicates the substrate's permittivity, ϵ_{eff} refers to the effective permittivity of the substrate at a specific resonance frequency, h stands for the substrate's thickness, and Δ_L

accounts for the fringing field's edge effect on the patch. In addition, microstrip lines are suggested for managing the impedance and reflection coefficient of the antenna. The size of the microstrip line is significantly affected by the input impedance and the chosen resonant frequency. In this study, the input impedance is set to 50 ohms. The dimensions of the microstrip line can be calculated using the following equation [22]:

$$W_z = \frac{2h}{\pi} \left\{ \frac{B - 1 - \ln(2B - 1) + \frac{\epsilon_r - 1}{2\epsilon_r} \left[\ln(B - 1) + 0.39 - \frac{0.61}{\epsilon_r} \right]}{B} \right\}, \tag{6}$$

$$B = \frac{60\pi^2}{Z_o\sqrt{\epsilon_{eff}}}. \tag{7}$$

In this context, W_z represents the width of the microstrip line, π is constant, Z_o denotes the antenna's impedance, and B stands for the impedance constant. The antenna's impedance is 50 Ω , matching the impedance of the connector used. Additionally, the length of the microstrip line (L_z) is $\frac{1}{4}$ of the wavelength (λ_g), calculated using the following equation [21]:

$$L_z = \frac{1}{4}\lambda_g, \tag{8}$$

$$\lambda_g = \frac{\lambda}{\epsilon_{eff}}. \tag{9}$$

The structure and simulation results of an antenna with a single element are shown in Fig. 2.

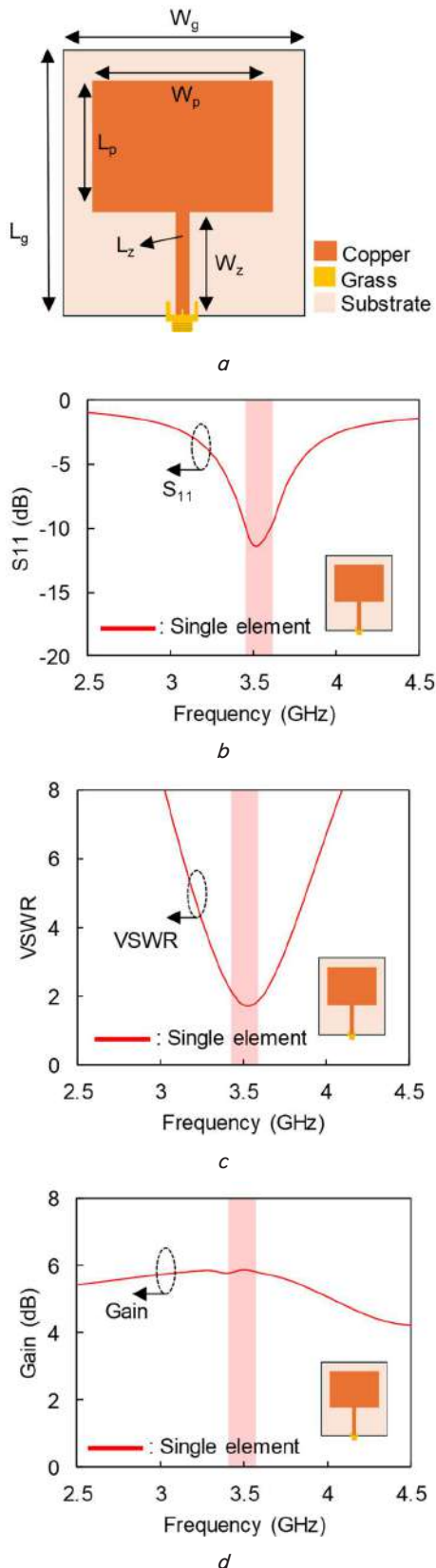


Fig. 2. Model of a single-element antenna: *a* – design of a single element; *b* – simulation of S_{11} ; *c* – simulation of VSWR; *d* – simulation of gain

Fig. 2, *a* shows the dimensions of W_p and L_p being 26 mm and 22 mm, respectively. In addition, the length and width of the microstrip lines represented by L_z and W_z are

13 mm and 3 mm. The dimensions of the ground plane are shown by W_g and L_g where the width and length are 35 mm and 29 mm. Furthermore, the simulation results of S_{11} , VSWR in Fig. 2, *a, b* show that the antenna has been operating at a resonance frequency of 3.5 GHz with S_{11} -11.34 dB and VSWR 1.74. The gain of the single-element antenna is shown in Fig. 2, *c* where the peak gain at a resonance frequency of 3.5 GHz is 5.8 dB. However, the bandwidth obtained from the single-element antenna is still narrow at 40 MHz (3.48–3.52 GHz). Therefore, optimization is required to increase the bandwidth of the proposed antenna.

The second stage is to optimize the single-element antenna into a series array antenna with two elements. The purpose of adding elements is to increase the gain while the bandwidth of the antenna is optimized with a spiral-shaped stub. The structure and simulation results of an array antenna with two elements are shown in Fig. 3.

Fig. 3, *a* shows the structure of an array antenna with two elements, where the dimensions of W_g and L_g are 32 mm and 71 mm. Moreover, spiral stubs are proposed to connect between elements with lengths L_1 , L_2 and L_3 of 6 mm, 7 mm and 6 mm. Furthermore, the width of the spiral stub is represented by W_b and W_s where the width is 3 mm and 1 mm, respectively. The simulation results of S_{11} and VSWR for an array antenna with two elements are shown in Fig. 3, *b, c* where S_{11} is -16.79 dB and VSWR is 1.33 at a resonance frequency of 3.5 GHz. The bandwidth obtained from the antenna array with two elements is 400 MHz (3.2–3.6 GHz) with a peak gain of 7.82 dB. This finding shows that the spiral stub and the addition of elements succeed in increasing the bandwidth and gain of the proposed antenna. However, the gain obtained is still low so further optimization is required. Therefore, the gain of the proposed antenna is optimized by increasing the number of elements of the array.

The third stage is to increase the antenna gain by optimizing the antenna array into four elements. The structure and simulation results of an array antenna with four elements are shown in Fig. 4.

Fig. 4, *a* illustrates the design of a four-element array antenna, with W_g and L_g of 32 mm and 142 mm, respectively. The array elements are linked by spiral stubs that extend in opposite directions. Furthermore, the simulation of S_{11} and VSWR shows that the antenna has high performance with S_{11} and VSWR of -29.28 dB and 1.07 at a resonance frequency of 3.5 GHz as shown in Fig. 4, *b, c*. The bandwidth obtained from the antenna array with four elements is 300 MHz (3.3–3.6 GHz) with a peak gain of 9.9 dB at a resonance frequency of 3.5 GHz as illustrated in Fig. 4, *d*.

The fourth stage is to optimize the antenna array with eight elements to increase the gain. Furthermore, an inset feed is proposed to control the resonant frequency of the antenna represented by W_i and W_d with dimensions of 7 mm and 1 mm, respectively. The length and width of the ground plane represented by W_g and L_g are 32 mm and 310 mm as shown in Fig. 5, *a*.

The simulation of S_{11} and VSWR of the array antenna with eight elements illustrated in Fig. 5, *b, c* shows that the antenna has been operating at a resonance frequency of 3.5 GHz with S_{11} of -26.37 dB and VSWR of 1.10. The bandwidth obtained is 300 MHz (3.3–3.6 GHz) while the peak gain is 10.82 dB at a resonance frequency of 3.5 GHz as shown in Fig. 5, *d*. Furthermore, the simulation results of S_{11} and the gain of the entire antenna model shown in Fig. 6, *a, b* are proposed to evaluate the optimization of the proposed antenna, respectively.

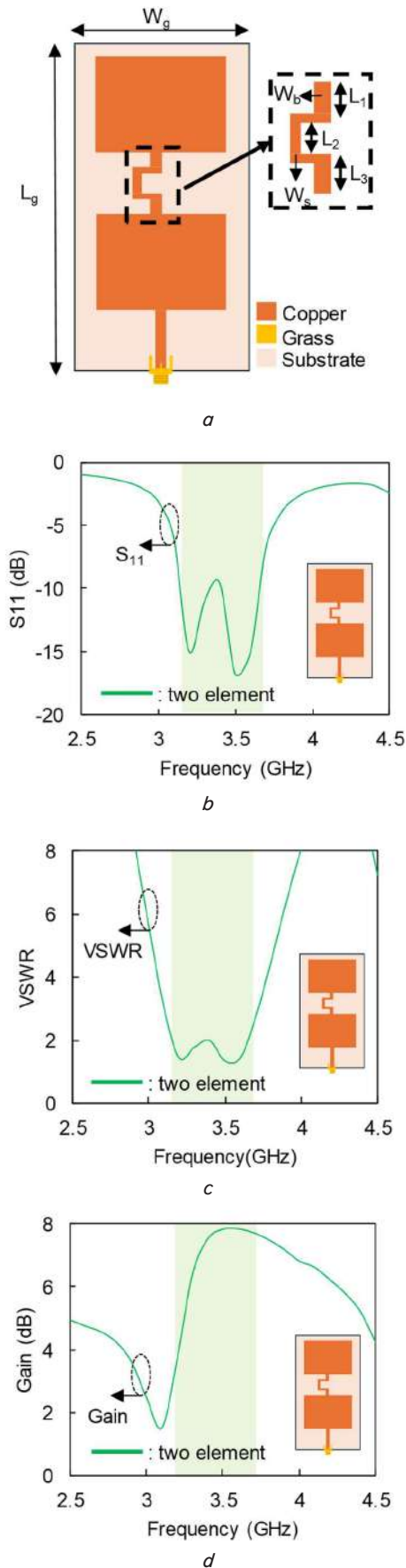


Fig. 3. Model of an array antenna with two elements: *a* – design of a two-element array with a spiral stub; *b* – simulation of S_{11} ; *c* – simulation of VSWR; *d* – simulation of gain

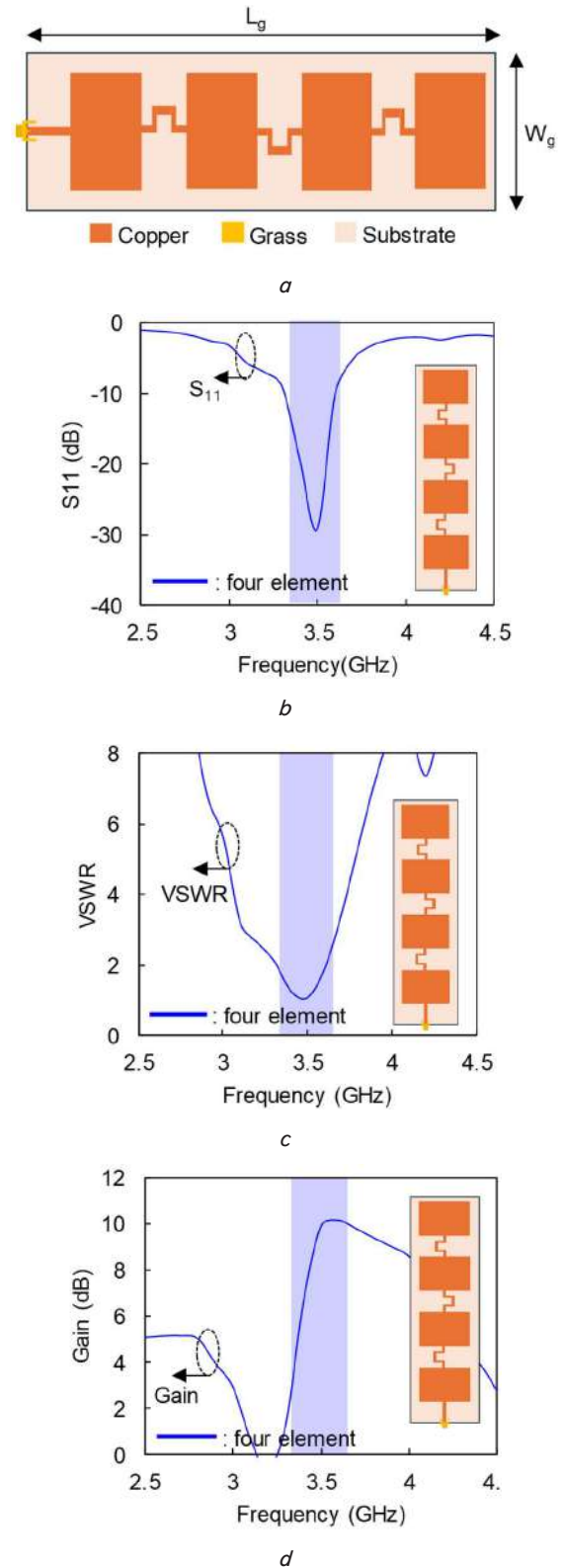


Fig. 4. Model of an array antenna with four elements: *a* – design of a four-element array with a spiral stub; *b* – simulation of S_{11} ; *c* – simulation of VSWR; *d* – simulation of gain

Fig. 6, *a* illustrates that the reflection coefficient of the proposed antenna gradually improves from -11.23 dB to -26.27 dB at a resonance frequency of 3.5 GHz. This result indicates that the optimization using an eight-element array antenna, spiral stub, and inset feed effectively enhanced the

antenna's performance in terms of the reflection coefficient by up to 134 % compared to a single-element antenna.

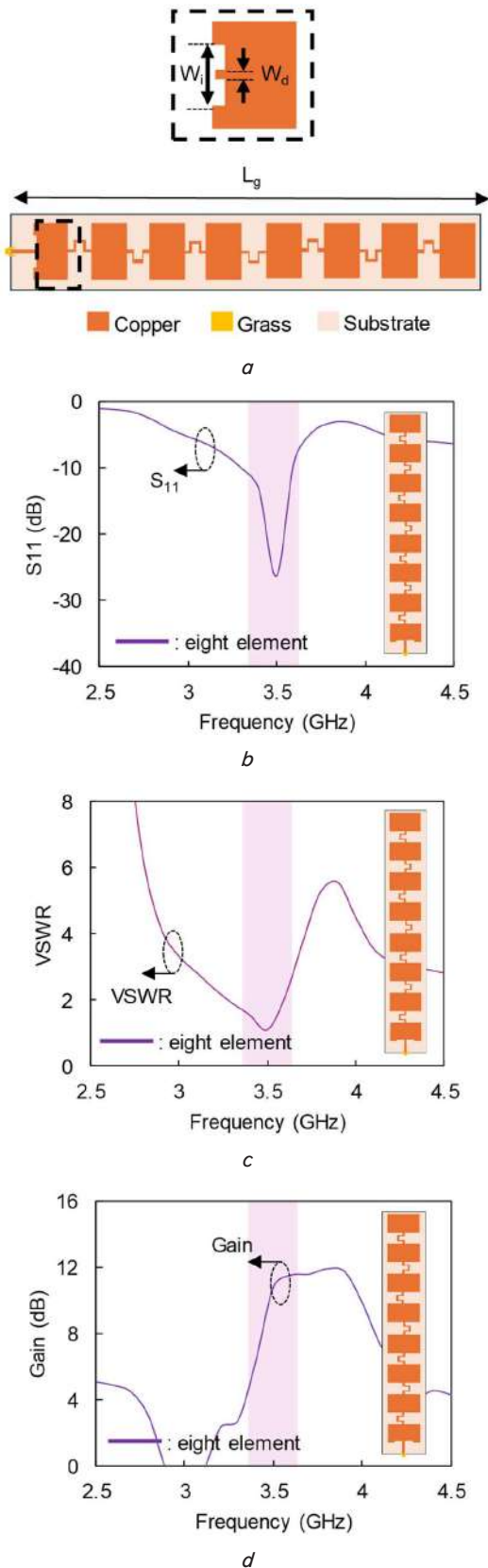


Fig. 5. Model of an array antenna with eight elements: *a* – design of an eight-element array with a spiral stub and inset fed; *b* – simulation of S_{11} ; *c* – simulation of VSWR; *d* – simulation of gain

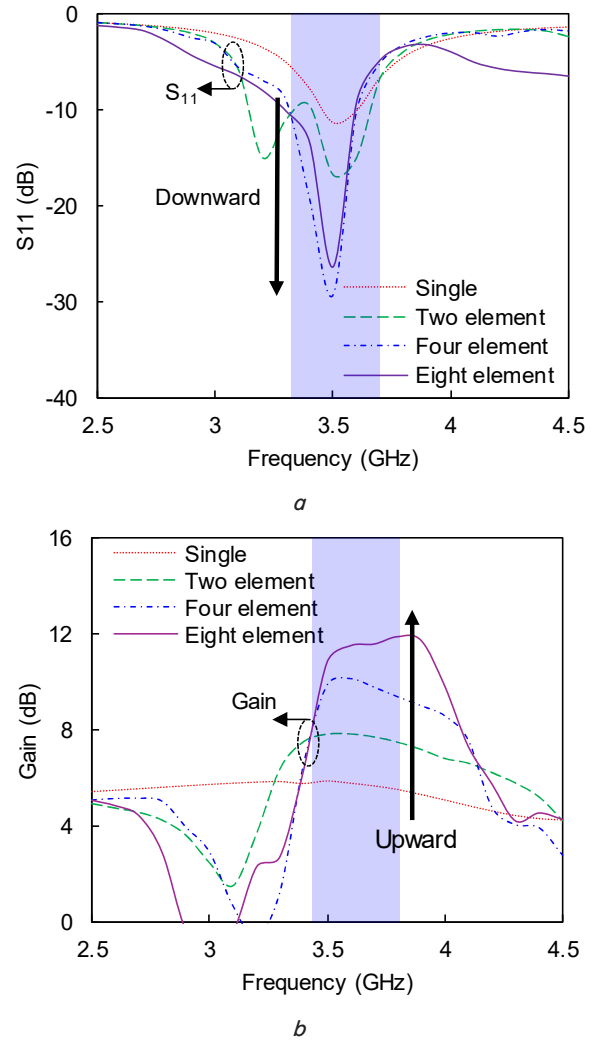


Fig. 6. Comparison of simulation results: *a* – simulation of S_{11} ; *b* – simulation of gain

Additionally, the bandwidth of the proposed antenna expanded by 650 %, from 40 MHz (3.48–3.52 GHz) to 300 MHz (3.3–3.6 GHz). This demonstrates that the proposed antenna meets the specifications for the 5G communication system operating within the 3.4–3.6 GHz frequency range. Moreover, Fig. 6, *b* shows that the antenna's gain increases as the number of elements in the antenna array is increased, with a gain improvement of 78 % from 5.8 dB to 10.82 dB at a resonance frequency of 3.5 GHz.

However, the gain of the proposed antenna remains below the desired target ≥ 12 dB. Thus, additional optimization is necessary to enhance the antenna's gain.

5. 2. Design of a MIMO series planar array antenna with 8x2 elements

In order to increase the gain, the antenna is configured as a series planar array with 8x2 elements. The elements of the antenna array are connected with impedance matching based on T-stubs while the antenna elements are optimized with slits on the right and left edges of the patch. The structure of the series planar array antenna and the simulation results are shown in Fig. 7.

Fig. 7, *a* shows the elements of the antenna separated by a certain distance represented by $d_a=21$ mm, which is determined based on the following equation [22]:

$$d_a = \frac{1}{8}\lambda, \tag{10}$$

$$\lambda = \frac{c}{f}, \tag{11}$$

where d_a is the distance between elements, λ is the wavelength of the antenna and c is the speed of light (3×10^8 m/s). It should be noted that the distance between the ele-

ments of a planar array antenna greatly affects the gain. Furthermore, microstrip lines with stepped impedance are used as impedance matching between elements of the antenna array represented by $Z_1=50 \Omega$, $Z_2=70.7 \Omega$ and $Z_3=100 \Omega$. The width of the transmission line dictates its impedance, which can be calculated using the following equation [21]:

$$Z_2 = \sqrt{Z_1 \cdot Z_3}. \tag{11}$$

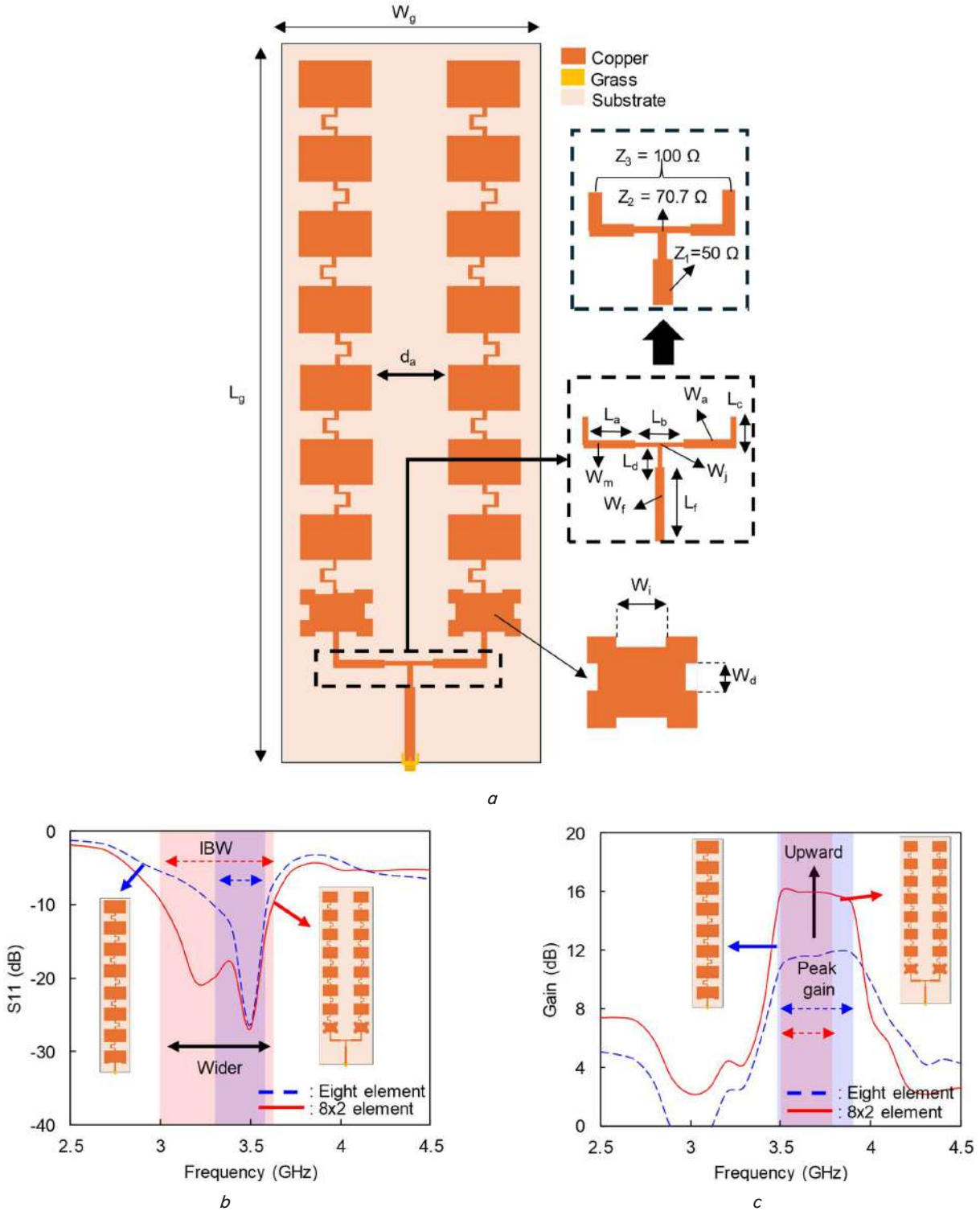


Fig. 7. Model of a series planar array antenna: *a* – design of an 8×2 element planar array with a spiral stub and inset feed; *b* – simulation of S_{11} ; *c* – simulation of VSWR; *d* – simulation of gain

The width of the microstrip line with stepped impedance is represented by $W_f=3$ mm, $W_j=1$ mm and $W_m=2$ mm while the length is represented by $L_f=33$ mm, $L_d=8$ mm, $L_b=23$ mm, $L_a=12$ mm and $L_c=17$ mm. The dimensions of the ground plane indicated by W_g and L_g are 82 mm and 353 mm, respectively. Furthermore, Fig. 7, *b* shows that the bandwidth of the proposed antenna increases from

300 MHz (3.3–3.6 GHz) to 600 MHz (3–3.6 GHz). In addition, the peak gain of the antenna also increases from 10.82 to 16.09 dB at a resonant frequency of 3.5 GHz as shown in Fig. 7, *c*. These findings indicate that the proposed antenna has met the specifications for a 5G communication system with a bandwidth of ≤ 200 MHz and a gain of ≥ 12 dB at a resonant frequency of 3.5 GHz.

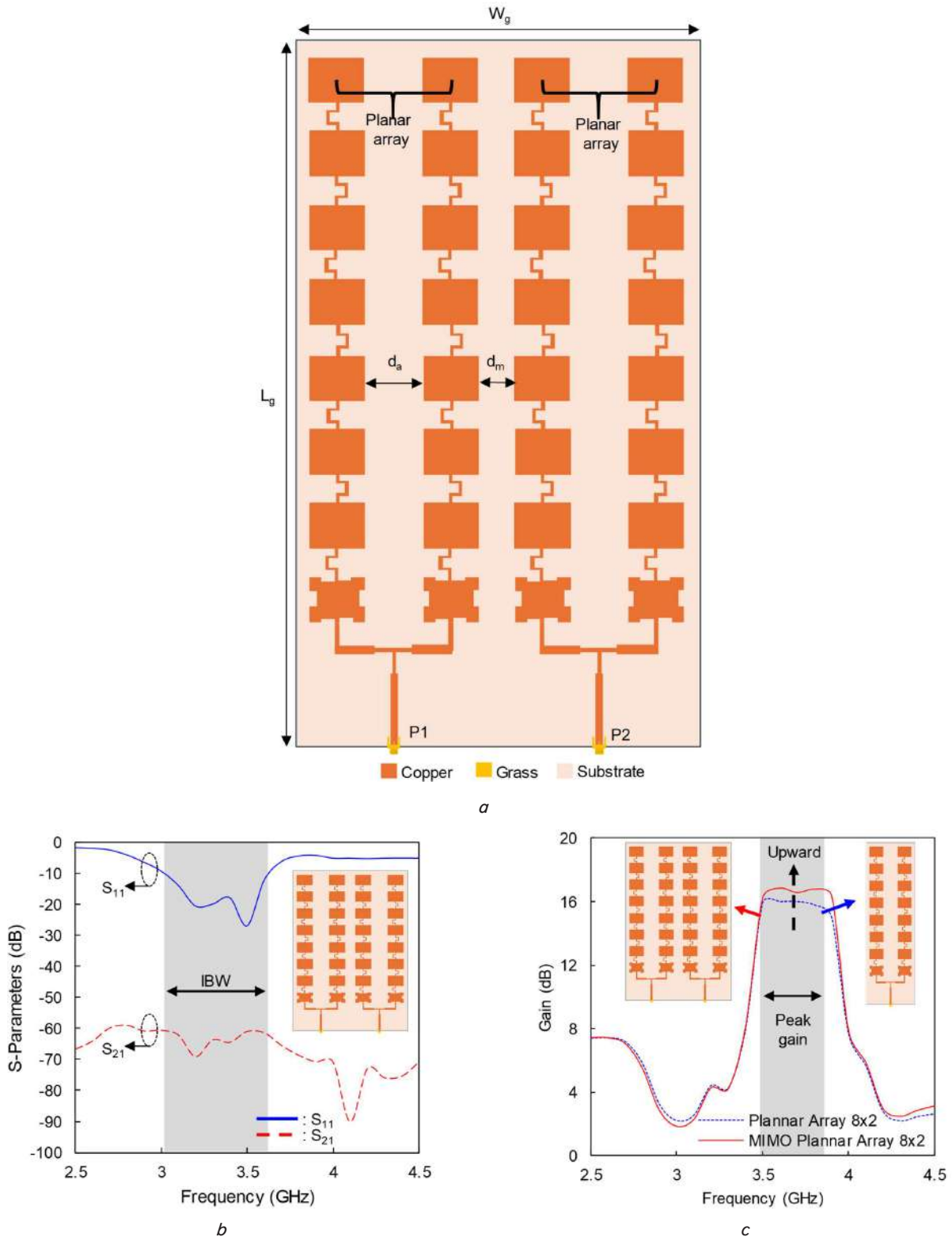


Fig. 8. Model of a MIMO series planar array antenna: *a* – design of an 8×2 element MIMO planar array; *b* – simulation of S_{11} ; *c* – simulation of VSWR; *d* – simulation of gain

The next step is to optimize the antenna with a MIMO configuration that is directly connected to port 1 and port 2, respectively. It should be noted that the distance between the antennas at each port greatly affects the mutual coupling of the MIMO configuration. Mutual coupling shows the independence of the antennas when both works simultaneously. The minimum standard for mutual coupling is $S_{21} \leq -20$ dB at the specified resonant frequency.

Furthermore, to support the 5G communication system, the antenna is configured in MIMO with 2 different ports represented by port 1 (P1) and port 2 (P2) as shown in Fig. 8, *a*. The structure of the series planar antenna array is connected to P1 and P2, respectively. In order to control the independence of the two antennas with high mutual coupling, the antennas are separated by a certain distance represented by $d_m = 21$ mm. The dimensions of the ground plane are represented by W_g and L_g , which are 164 mm and 353 mm, respectively.

The simulation results illustrated in Fig. 8, *b* show that the antenna has been operating at a resonant frequency of 3.5 GHz with S_{11} and S_{21} around -20 dB and -60 dB with a bandwidth of 650 MHz (3–3.65 GHz). This finding indicates that the antenna has a bandwidth that meets the criteria for the 5G communication system and has high mutual coupling with $S_{21} \leq -20$ dB. In addition, the gain of the antenna with MIMO configuration also increases from 15.98 dB to 16.78 dB as shown in Fig. 8, *c*. This shows that the proposed antenna has met the specifications for 5G communication systems where the gain is ≥ 12 dB. The next stage is to fabricate and validate the performance of the proposed antenna through a measurement process in the laboratory.

5.3. Validation and measurement of the proposed antenna

The antenna is fabricated using an FR-4 substrate where the radiating element is located on the top layer while the bottom layer functions as a ground plane as shown in Fig. 9, *c*. Validation of the near-field performance is carried out through a measurement process using a Vector Network Analyzer (VNA) with a frequency range of 2.5–4.5 GHz, a frequency step size of 0.01 GHz and a temperature of 25°, which is connected to the antenna (AUT) via port 1 and port 2 with a coaxial cable as shown in Fig. 9, *a*.

The measurement setup consists of an antenna under test (AUT), which functions as a transmitter (T_x) connected to an RF generator while a reference antenna is placed as a receiver (R_x) connected to a spectrum analyzer and separated based on the Fresnel zone where $d_f = 2D^2/\lambda$ [20]. The antenna is placed on a rotator that rotates clockwise from 0–360° with a step size of 1°. The far-field characteristics of the proposed antenna are observed based on the antenna’s radiation pattern when transmitting and receiving electromagnetic waves.

A comparison of the simulation and measurement results of S_{11} and S_{21} in Fig. 10, *a* show that the fabricated antenna has the same performance as the simulated antenna where S_{11} is around -20 dB while S_{21} is around -40 dB at a resonance frequency of 3.5 GHz. The bandwidth of the fabricated antenna is 680 MHz with a frequency range

of 3–3.68 GHz. This finding shows that the measurement results are in line with the simulation results.

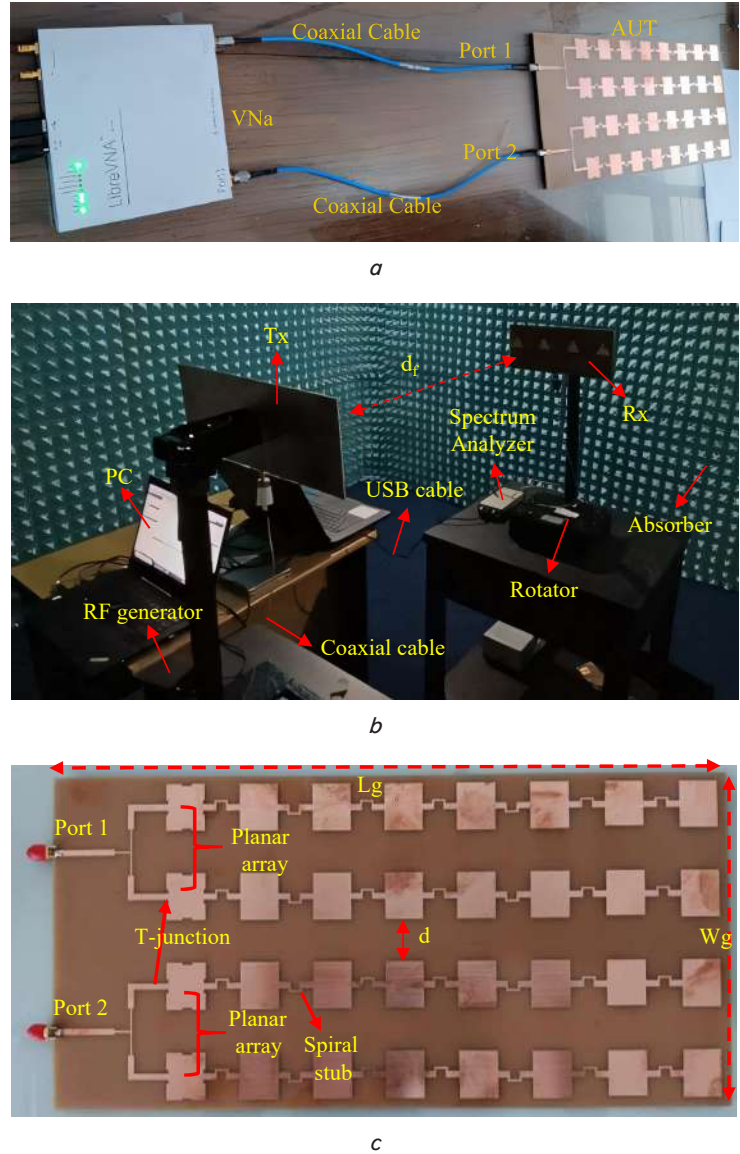


Fig. 9. Measurement process of the proposed antenna: *a* – measurement setup for near-field validation; *b* – measurement setup for far-field validation in an anechoic chamber; *c* – fabrication of the proposed antenna

The subsequent phase involves assessing the performance of the MIMO antenna by examining the Envelope Correlation Coefficient (ECC) and Diversity Gain (DG) parameters. The ECC quantifies the correlation between the two antennas operating in tandem within a MIMO configuration. Typically, the ECC value lies within the range of 0 to 1, with a threshold of ≤ 0.5 generally accepted for MIMO antenna designs. The ECC can be calculated using the following equation [20]:

$$ECC = \frac{|S_{11}^* S_{12} + S_{21}^* S_{22}|^2}{(1 - |S_{11}|^2 - |S_{21}|^2)(1 - |S_{22}|^2 - |S_{12}|^2)} \quad (12)$$

Diversity Gain (DG) characterizes the capability of an antenna system to mitigate the effects of multipath fading.

The DG value reflects the system’s ability to enhance or sustain the signal quality relative to noise by combining signals from multiple antennas rather than relying on a single antenna. For MIMO antennas, the diversity is typically represented by a DG value of ≤ 10 dB [18]. The DG can be calculated using the following equation [20]:

$$DG = 10\sqrt{1 - (ECC)^2}. \tag{13}$$

Fig. 10, *b* shows that the fabricated antenna has ECC and DG of about 0–0.001 dB and 9.99–10 dB in the resonant frequency range of 2.5–4.5 GHz. This finding indicates that the proposed antenna has high independence and diversity. Additionally, high diversity gain contributes to better data throughput and coverage, making the antenna system more efficient in delivering consistent performance in challenging conditions, such as urban environments or areas with obstacles.

To validate the independence and mutual coupling of the proposed antenna, a comprehensive observation of the electric field concentration by EM simulation is proposed as shown in Fig. 11, *a*. The electric field of the proposed antenna is observed at a resonant frequency of 3.5 GHz and shows that the resulting mutual coupling is low as indicated by the highest electric field only at the antenna at port 1 (P1) and does not distribute the electric field to the antenna at port 2 (P2).

Furthermore, the beamforming of the proposed antenna is shown in Fig. 11, *b* where the main lobe radiates electromagnetic waves to the front of the antenna while the side lobes radiate to the top, bottom and back of the antenna. Furthermore, the radiation pattern of the simulation and measurement process illustrated in Fig. 11, *c* shows a straight and similar result where the maximum radiation is at an angle of 0 with a transmit power of about 17.8 dB. This finding indicates that the proposed antenna has operated optimally at a resonance frequency of 3.5 GHz and supports MIMO for 5G communication systems. Moreover, a comparison of bandwidth and gain for the development models of the proposed antenna is shown in Tables 1, 2.

The bandwidth and gain enhancement of the antenna can be determined using the following equation:

$$BW = \frac{(Optimized\ BW - Initial\ BW)}{Initial\ BW} \times 100\%, \tag{14}$$

$$Gain = \frac{(Optimized\ Gain - Initial\ Gain)}{Initial\ Gain} \times 100\%. \tag{15}$$

Table 1
Comparison of bandwidth for the proposed antenna models

Model	Frequency range (GHz)	Bandwidth (MHz)
1 st model	3.48–3.52	40
2 nd model	3.2–3.6	400
3 rd model	3.3–3.6	300
4 th model	3.3–3.6	300
5 th model	3–3.6	600
6 th model	3–3.65	650

Table 2
Comparison of gain for the proposed antenna models

Model	Frequency range (GHz)	Gain (dB)
1 st model	3.48–3.52	5.8
2 nd model	3.2–3.6	7.82
3 rd model	3.3–3.6	9.9
4 th model	3.3–3.6	10.8
5 th model	3–3.6	16.09
6 th model	3–3.65	17.8

Based on equation (14) and equation (15), the increase in gain and bandwidth is obtained by calculating the difference between the bandwidth and gain of the antenna with the initial condition and the optimized condition. In this study, the initial bandwidth and gain used are single-element antennas while the bandwidth and optimization gain are obtained from MIMO array antennas with 8×2 elements.

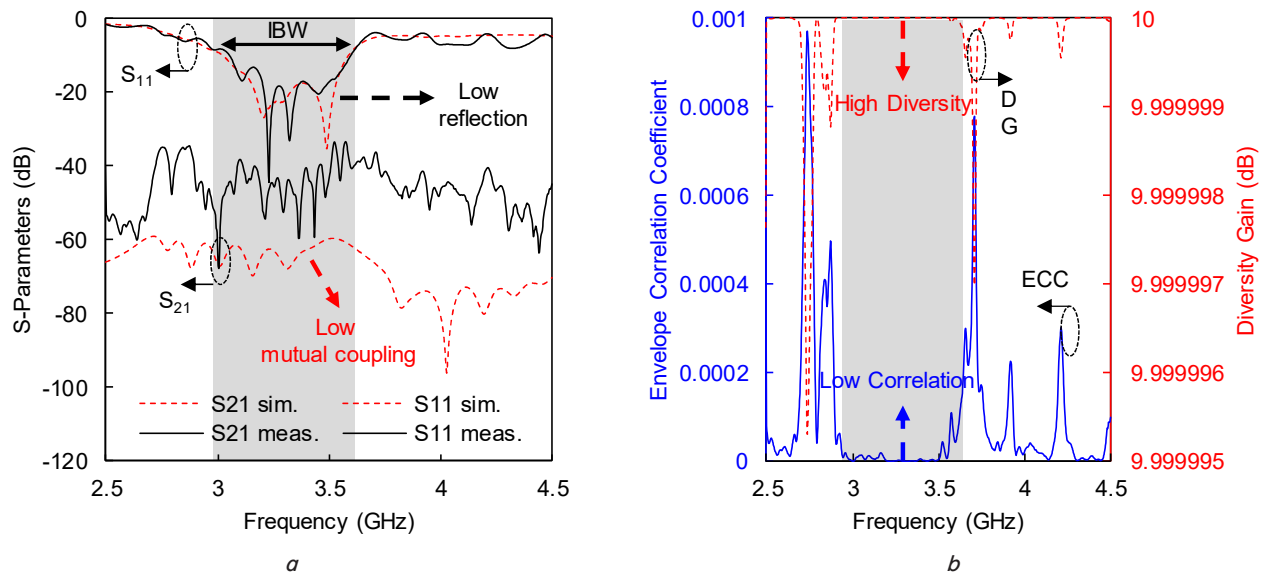


Fig. 10. Performance of the proposed antenna: *a* – comparison of the simulation and measurement results of S₁₁ and S₂₁; *b* – envelope correlation coefficient and diversity gain based on measurement results

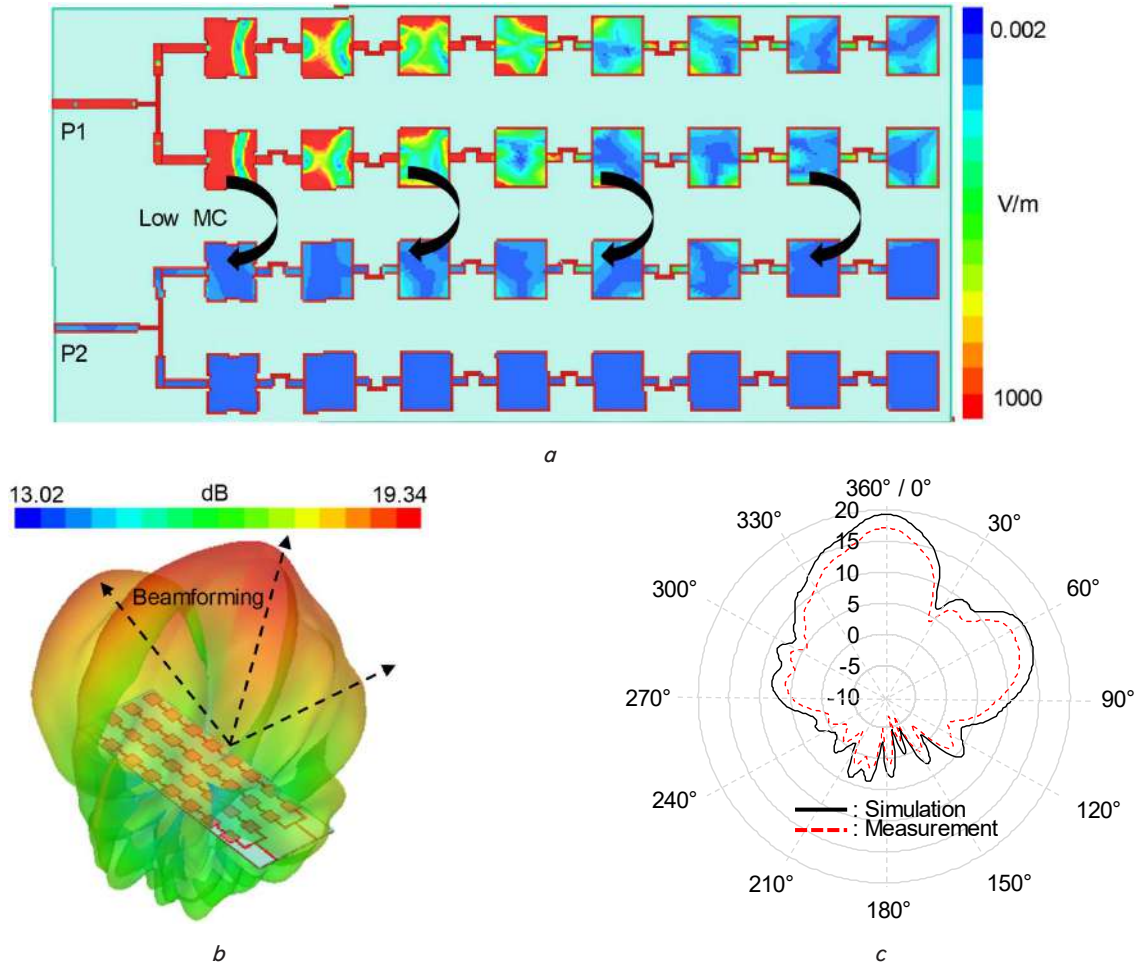


Fig. 11. MIMO performance of the proposed antenna: *a* – simulation of the E-field concentration of the proposed antenna at $f_r=3.5$ GHz; *b* – 3D simulation of the radiation of the proposed antenna at $f_r=3.5$ GHz; *c* – comparison of the simulation and measurement of the radiation pattern at $f_r=3.5$ GHz

6. Discussion of performance validation of the proposed MIMO antenna

Based on the measurement process, the comparison of the bandwidth of all the proposed antenna models is shown in Table 1. Based on Table 1, the bandwidth of the antenna with model 1 increases significantly from 40 MHz to 400 MHz in model 2 and 300 MHz in models 3 and 4. Furthermore, in models 5 and 6, the bandwidth increases to 600 MHz and 650 MHz. From the measurement results, it is found that the bandwidth of the antenna increases up to 1,525 % compared to the single-element antenna.

Furthermore, evaluation is also done by observing the gain of the proposed antenna. The gain comparison of the entire antenna model is shown in Table 2. Based on Table 2, the antenna gains increase in line with the addition of the number of elements of the antenna array. In model 1, the antenna gain is 5.8 dB while for model 2, model 3 and model 4, the antenna gains increase to 7.8 dB, 9.9 dB and 10.2 dB, respectively. Furthermore, in model 5 and model 6, the antenna gains increase to 16.09 and 17.8 dB.

Overall, the gain of the antenna increases up to 206.8 % compared to the single-element antenna. This finding shows that the evolution of the antenna has successfully improved the antenna performance by producing high gain. In addition, the MIMO performance of the antenna is shown with

high mutual coupling $S_{21} \leq -20$ dB. From the measurement results, a mutual coupling S_{21} of -40 dB was obtained in the frequency range of 2.5–4.5 GHz. MIMO performance is also indicated by high diversity with a diversity gain of 9.9 dB and a low correlation of 0.0001. This finding shows that the antennas have high independence and do not affect each other when working together.

From the results obtained, the proposed antenna has a performance with wide bandwidth and high gain compared to previous works [15–18]. In addition, the proposed antenna also has the capability for a high-performance MIMO system compared to the previous work [19], which proposed an antenna for a 5G communication system that does not support MIMO systems.

However, there are certain limitations, such as the relatively large antenna dimensions and its operation being restricted to a single resonant frequency. Consequently, future research efforts will focus on minimizing the antenna's dimensions and enhancing its performance across multiple resonant frequencies, enabling its application in other communication systems like 4G, Zigbee, and Wi-Fi.

7. Conclusions

1. From the measurement results, it was found that the proposed antenna has operated at a frequency of 3.5 GHz

with a wide bandwidth of 680 MHz. The bandwidth of the antenna has successfully met the standard requirements for a 5G communication system where the minimum bandwidth is ≤ 200 MHz.

2. The gain of the proposed antenna was successfully increased gradually using a series planar array with 8×2 elements. From the measurement results, a gain of 17.8 dB was obtained. This finding indicates that the proposed antenna has met the target with a gain of ≥ 12 dB for a 5G communication system.

3. The proposed antenna has been successfully developed with a two-port MIMO configuration operating at a resonant frequency of 3.5 GHz. From the measurement results, it was found that the proposed antenna has a high mutual coupling with S_{21} of -40 dB with ECC 0.001 and DG 9.99 dB. This finding indicates that the proposed antenna has met the criteria of high mutual coupling with $S_{21} \leq -20$ dB.

thorship or otherwise, that could affect the research, and its results presented in this paper.

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Data availability

The manuscript has no associated data.

Conflict of interest

The authors declare that they have no conflict of interest in relation to this research, whether financial, personal, au-

Use of artificial intelligence

The authors confirm that they did not use artificial intelligence technologies when creating the current work.

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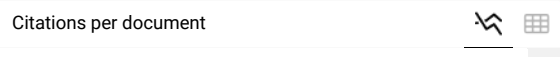
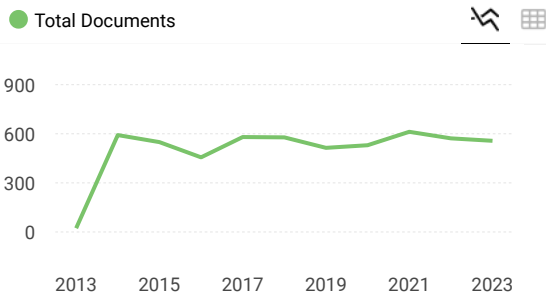
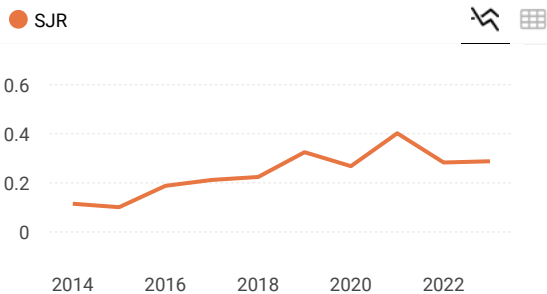
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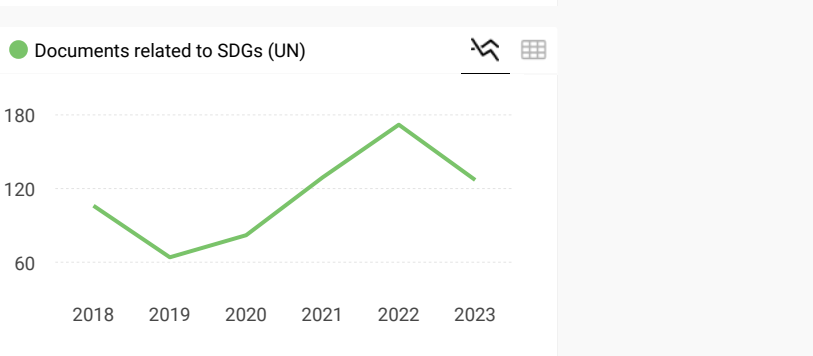
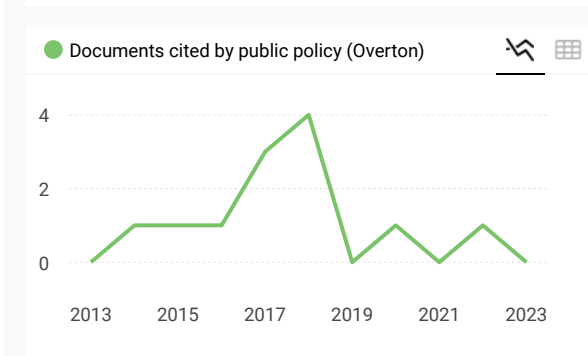
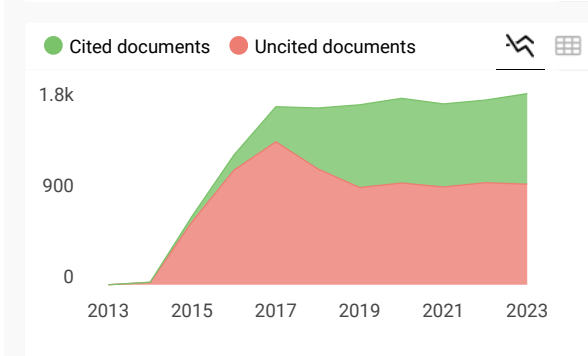
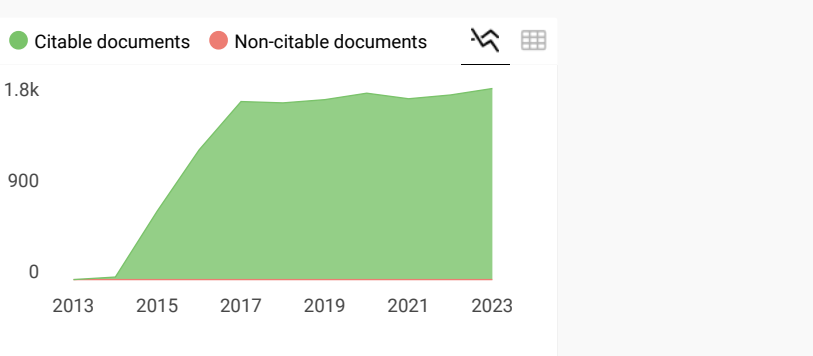
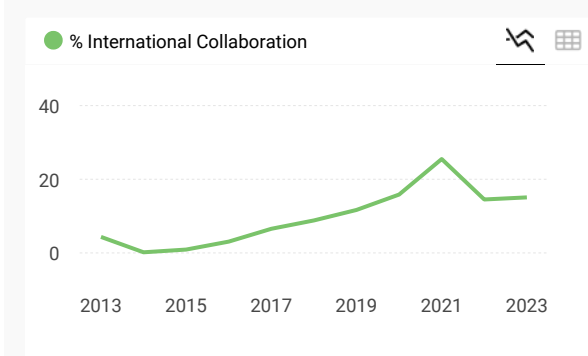
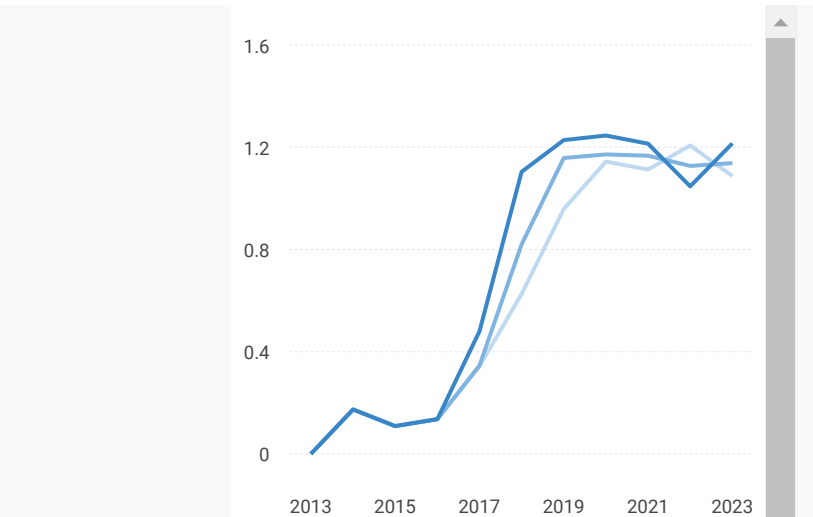
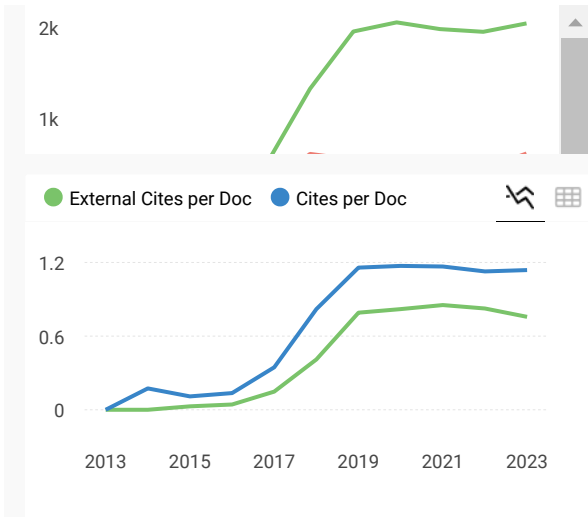
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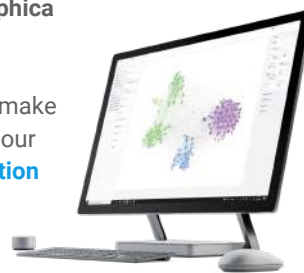
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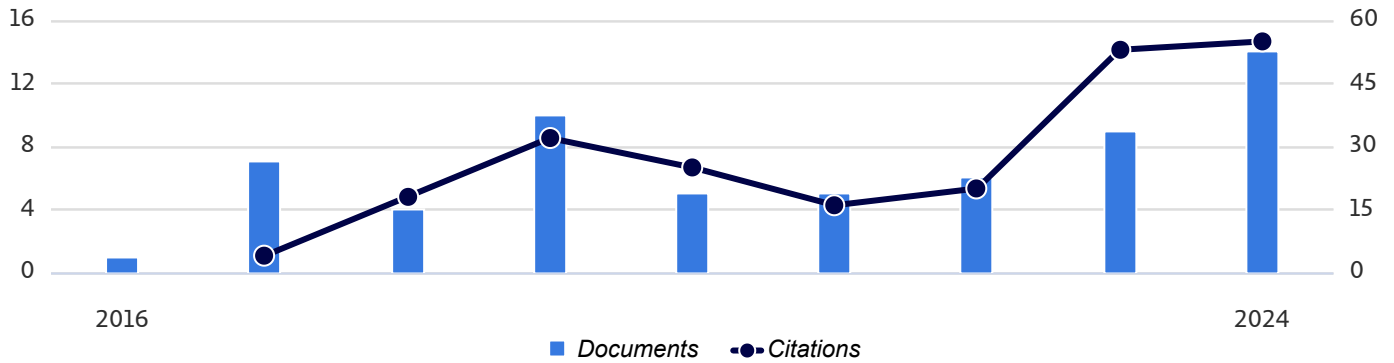
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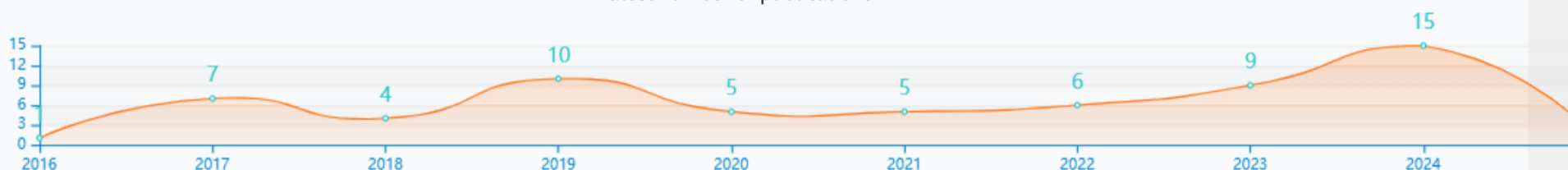


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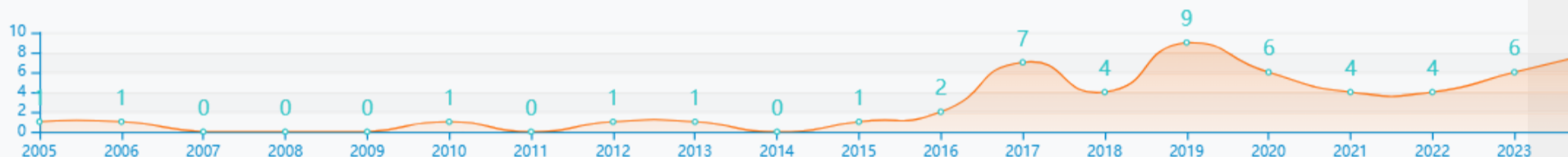
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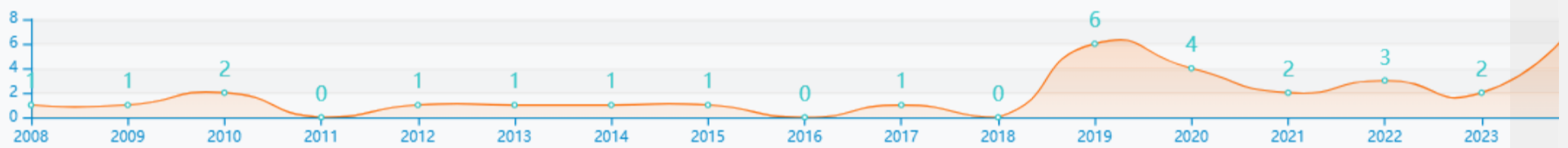
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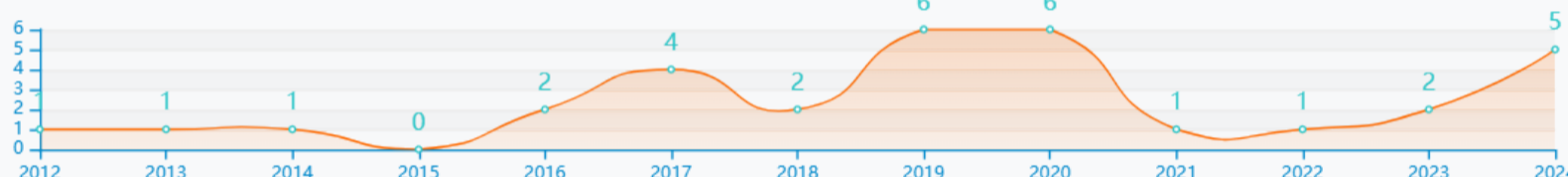
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